

# ADVANCED ROBOTICS

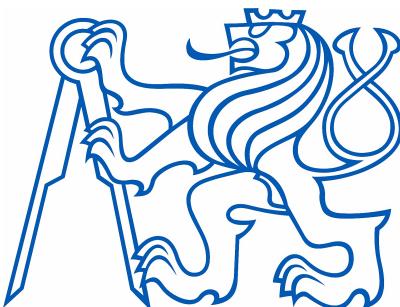


Tomas Pajdla  
2017



# Tomas Pajdla

Scholar in  
Computer Vision, Machine Learning, Robotics  
Applied Algebra & Geometry



**CIIRC**



Czech Technical University in Prague  
Czech Institute of Informatics, Robotics & Cybernetics  
Faculty of Electrical Engineering

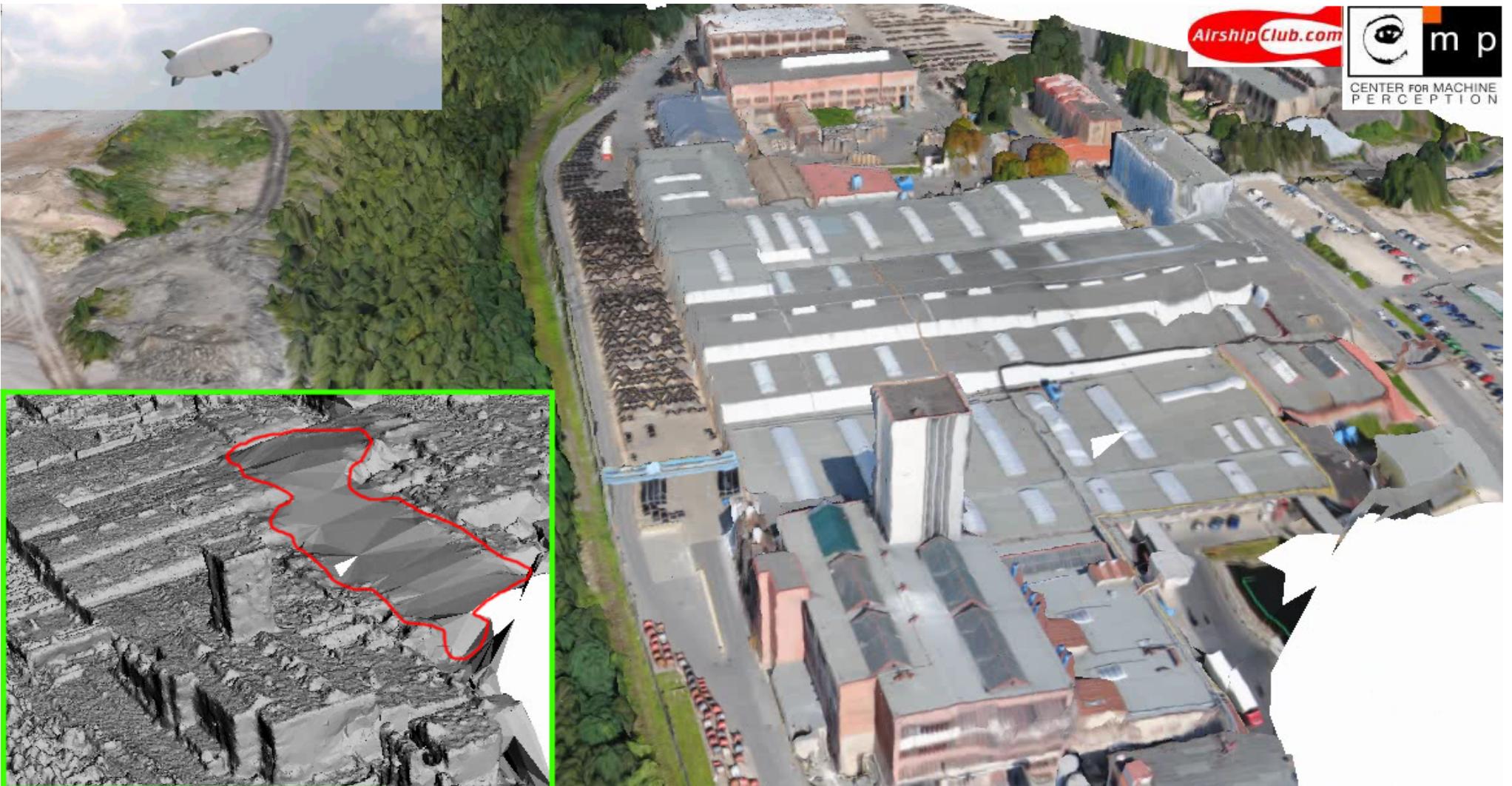
Czech Institute of Informatics, Robotics & Cybernetics  
Distinguished Researcher  
Head of Applied Algebra and Geometry Group

Faculty of Electrical Engineering  
Associate Professor

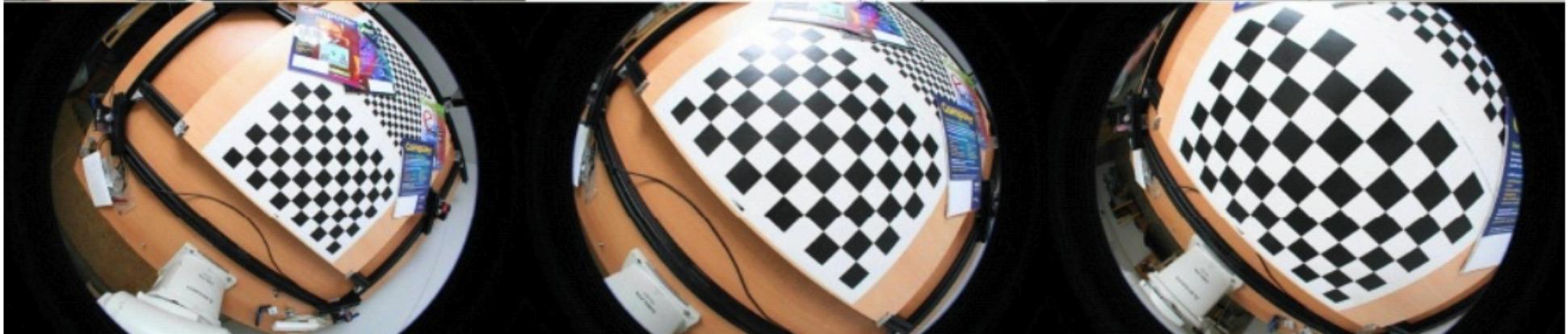


National Institute of Informatics Tokyo  
Visiting Associate Professor

# 3D Computer Vision

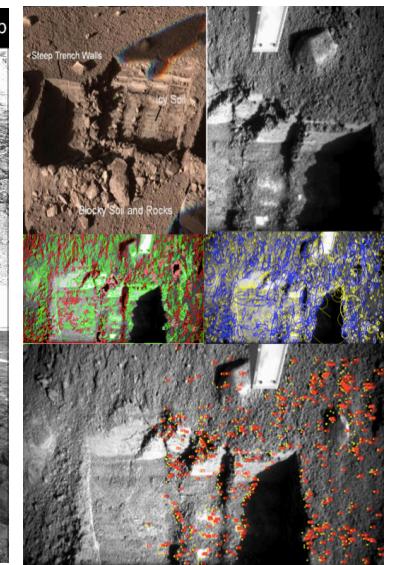
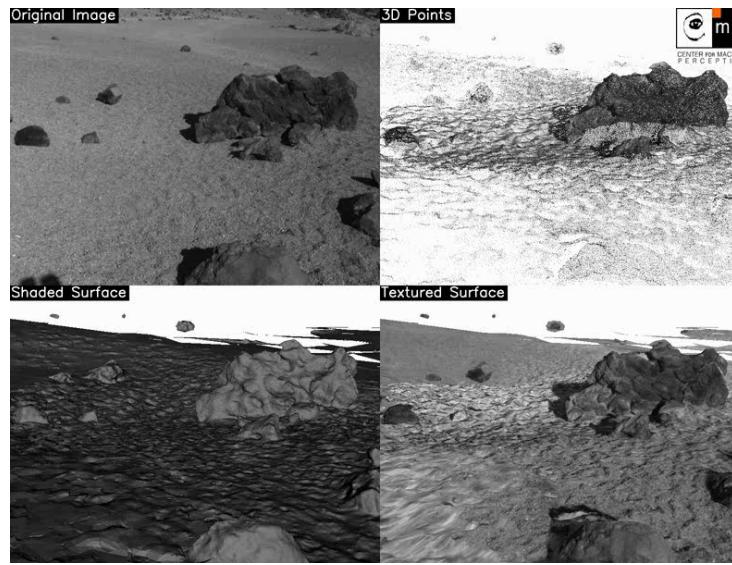
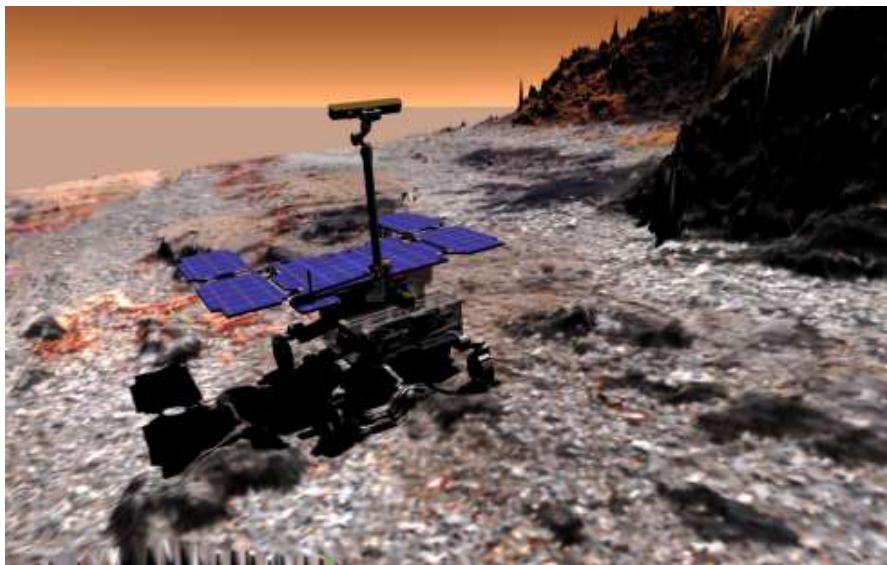
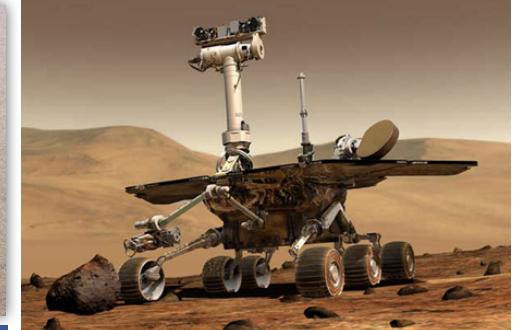


# Camera & Robot Calibration

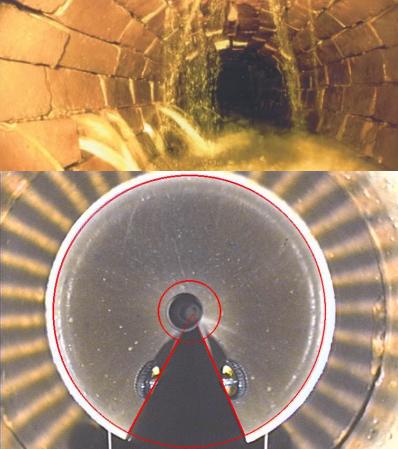
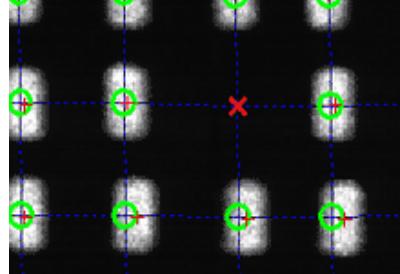
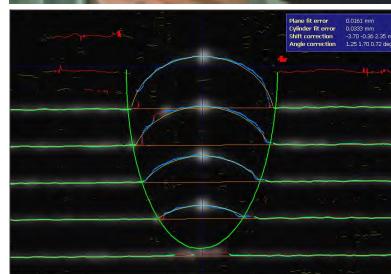
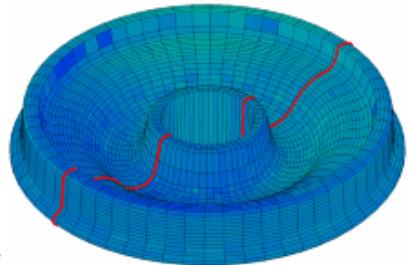
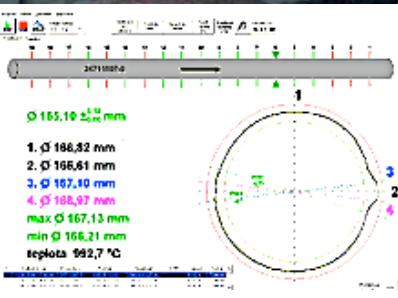
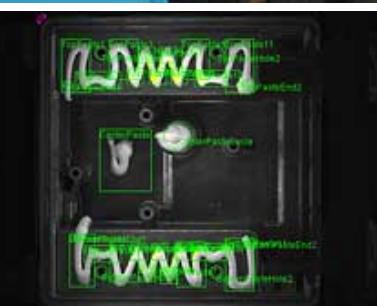
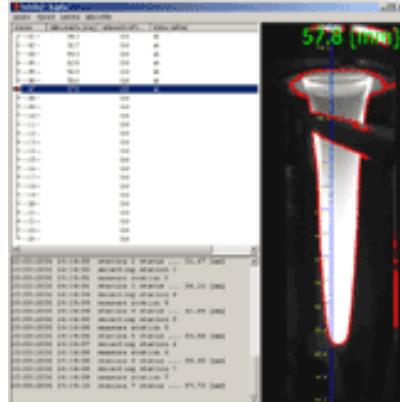
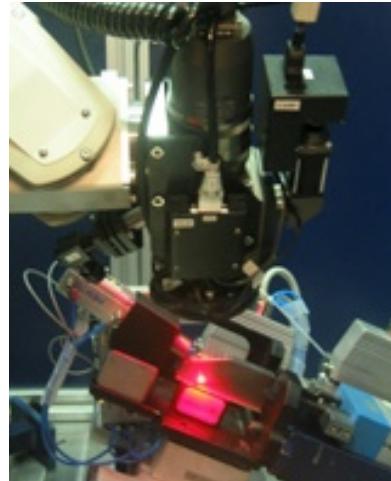
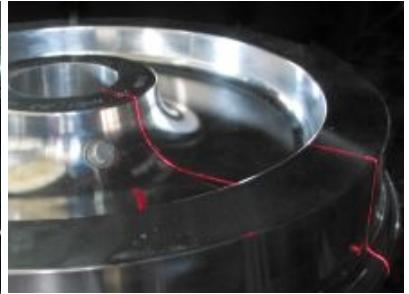


# Mobile Robotics

PRoVisG Field Trials Tenerife



# Computer Vision for Industry



# Advanced Robotics

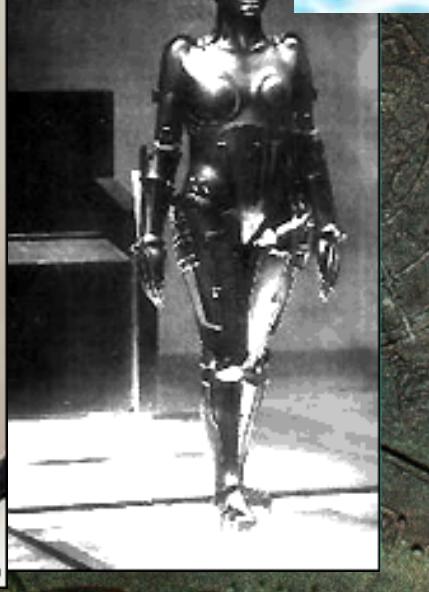
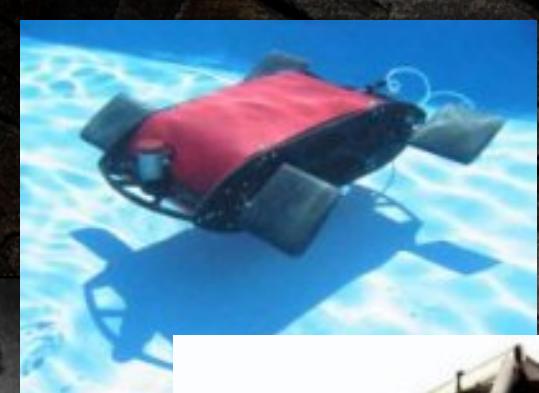
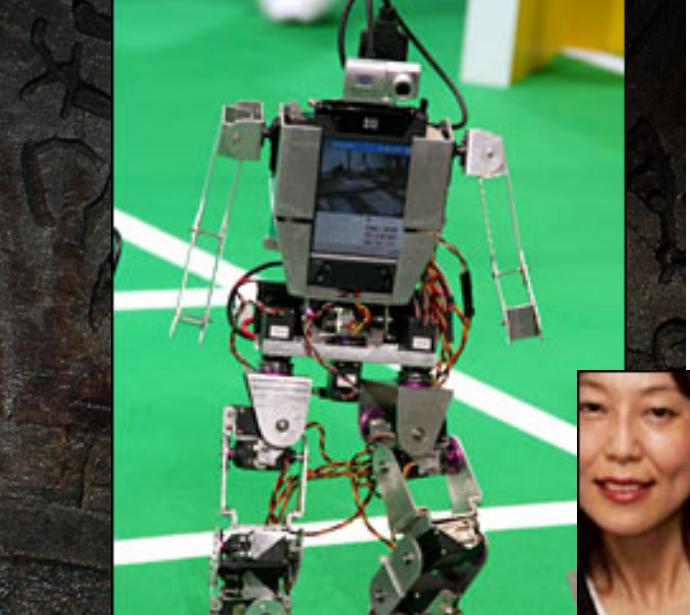
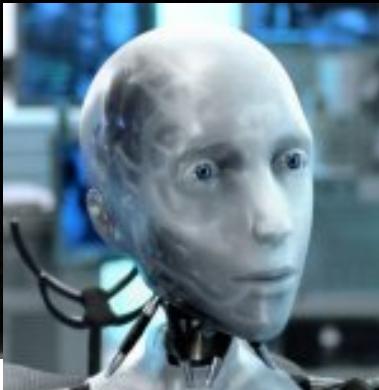
## Lecture 1

We will build on Robotics by V. Smutny and study more advanced robot kinematics problems, e.g.,

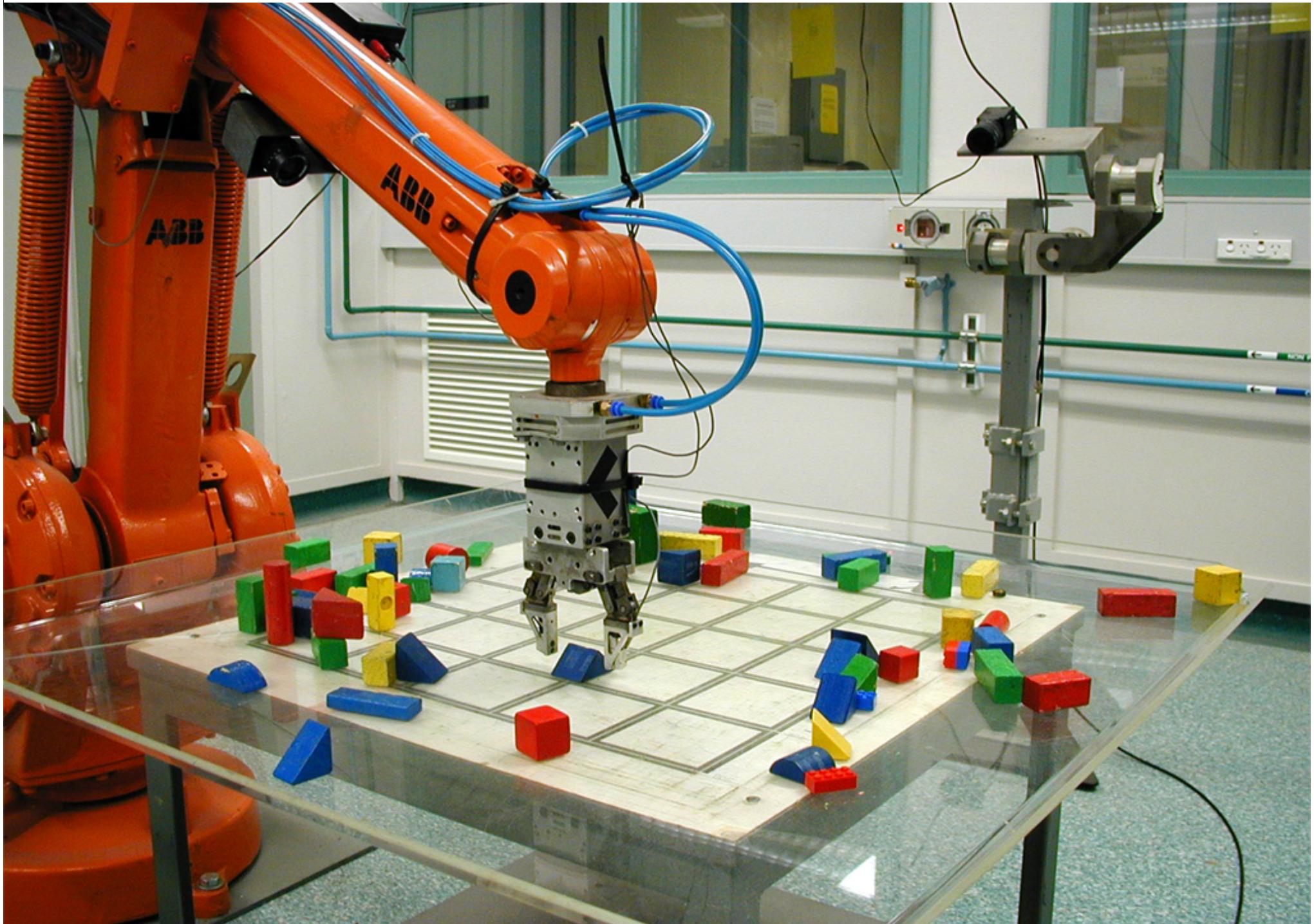
1. solving inverse kinematics of a general 6 DOF manipulator
2. identifying kinematic parameters of a manipulator
3. finding singular poses of a manipulator

with more advanced mathematical tools, such as

1. space rotation and motion and
2. solving algebraic equations



# ROBOT = A GENERAL MANIPULATOR

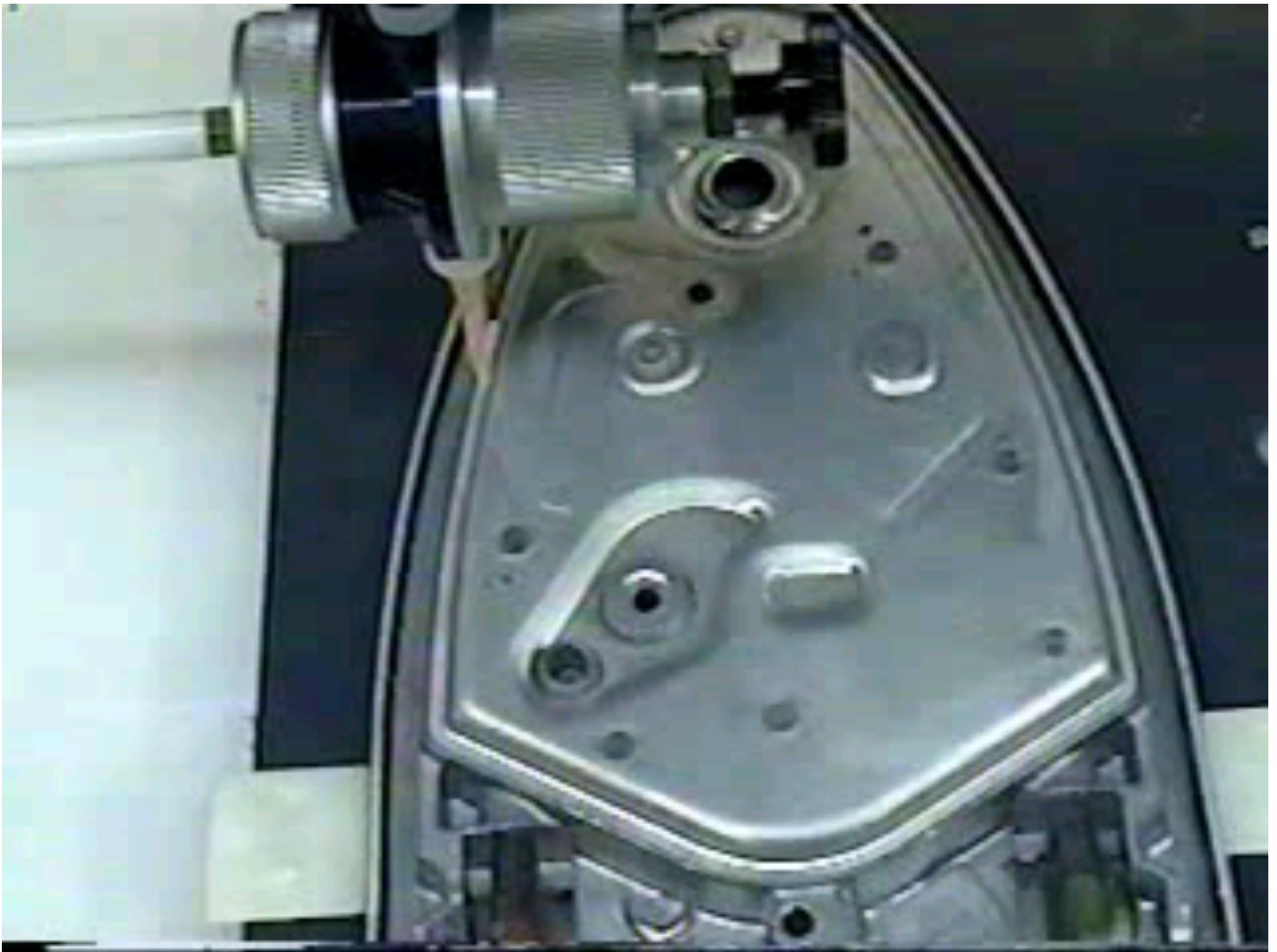


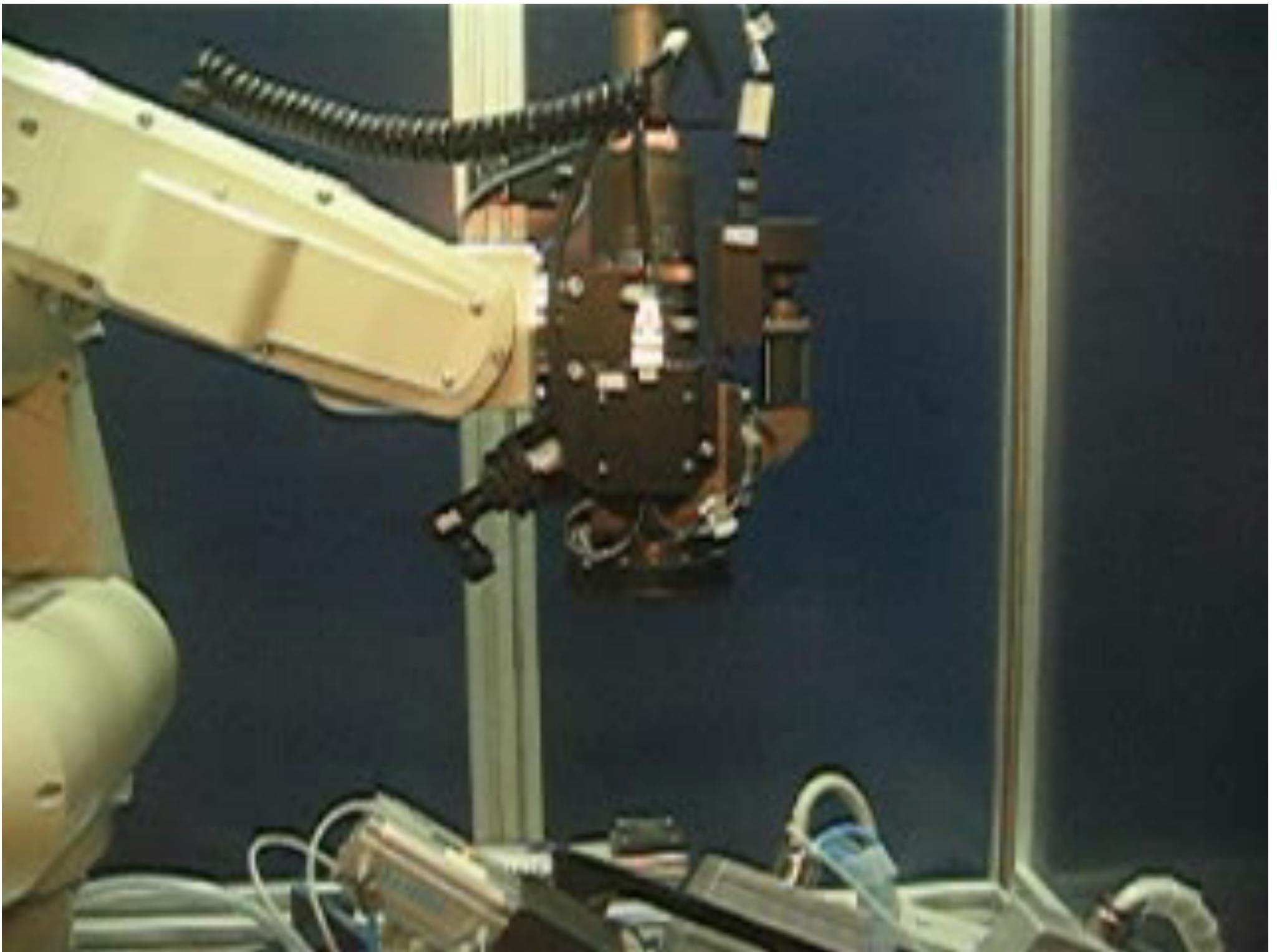
## Robotics

- [Go to The ABB Product Guide](#)
- [Robotics startpage](#)
- [+ Product range](#)
- [Application areas](#)
  - [Arc welding](#)
  - [Assembly](#)
  - [Foundry applications](#)
  - [Gluing and Sealing](#)
- [+ Material handling and Machine Tending](#)
- [Packing](#)
- [Palletizing](#)
- [Picking](#)
- [Painting and coating](#)
- [Spot welding](#)
- [Waterjet cutting](#)

## Application areas



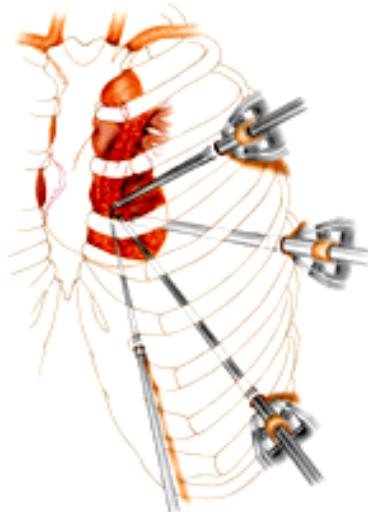




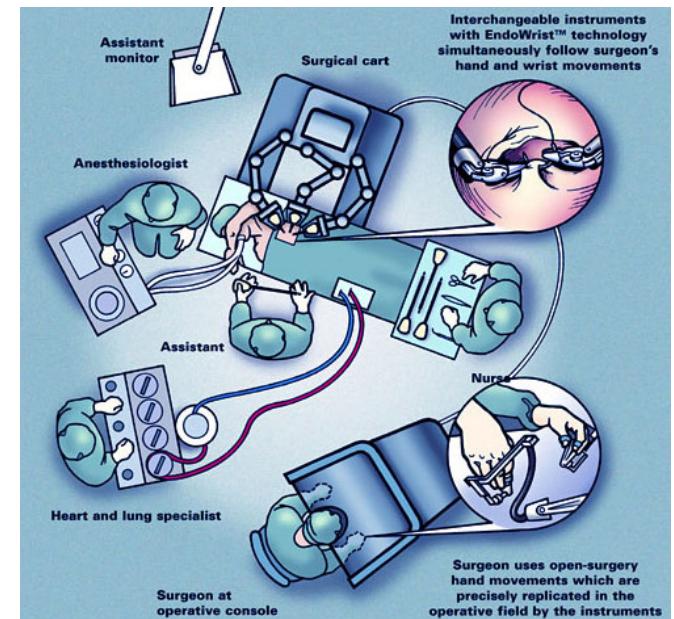
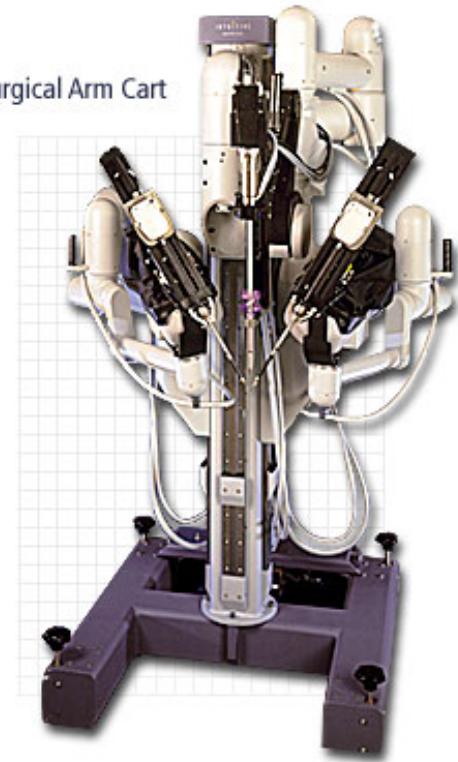




# Precision for robotic surgery



Surgical Arm Cart



<http://www.cts.usc.edu/rsi-article-robotputstuscatforefront.html>

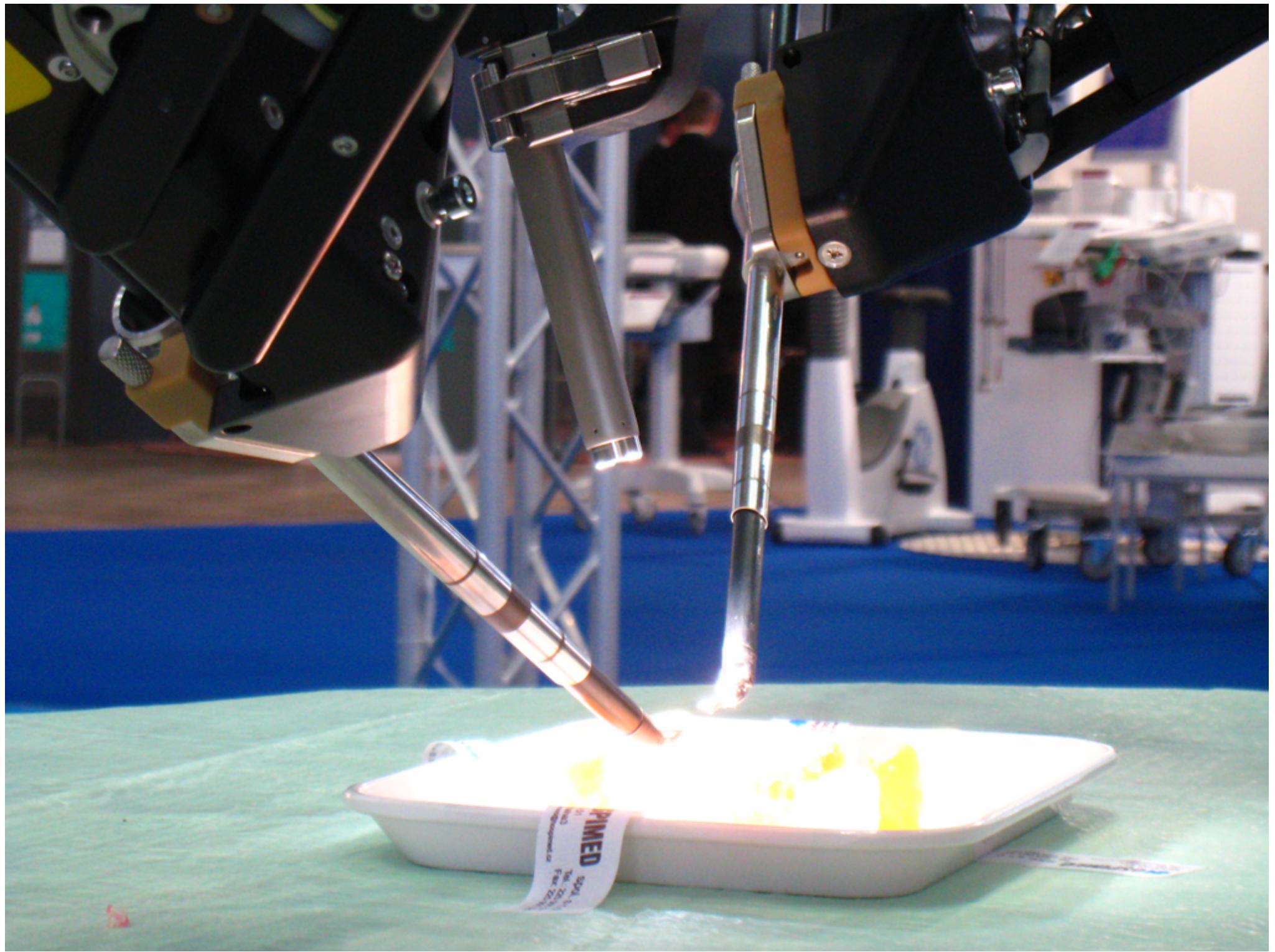
da Vinci®

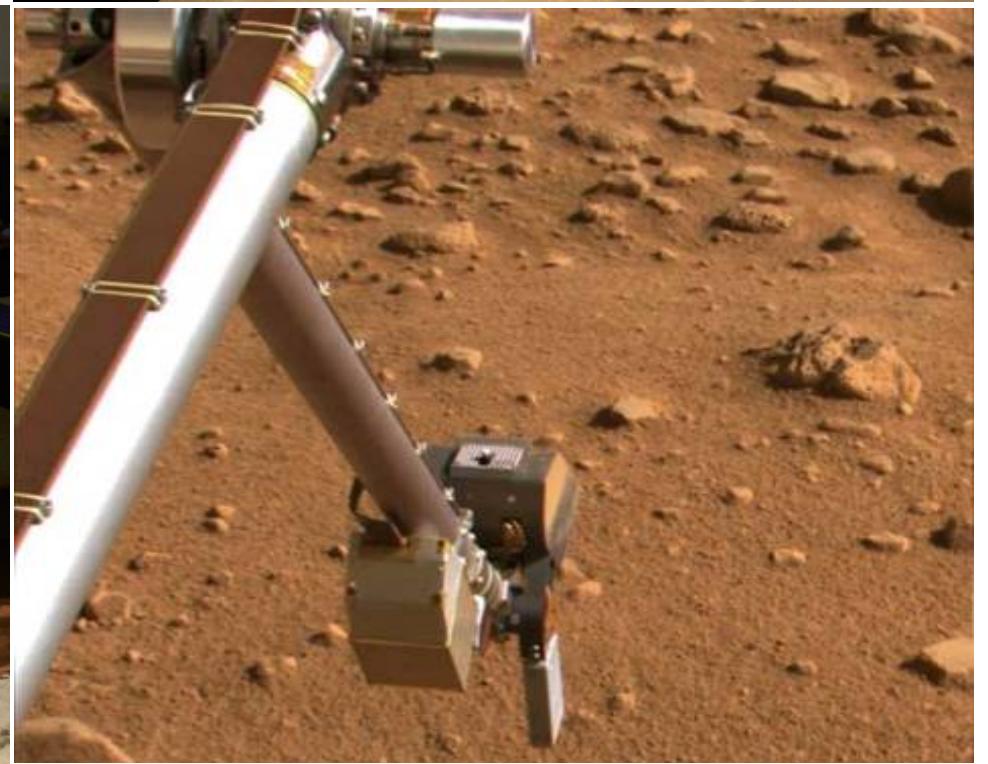
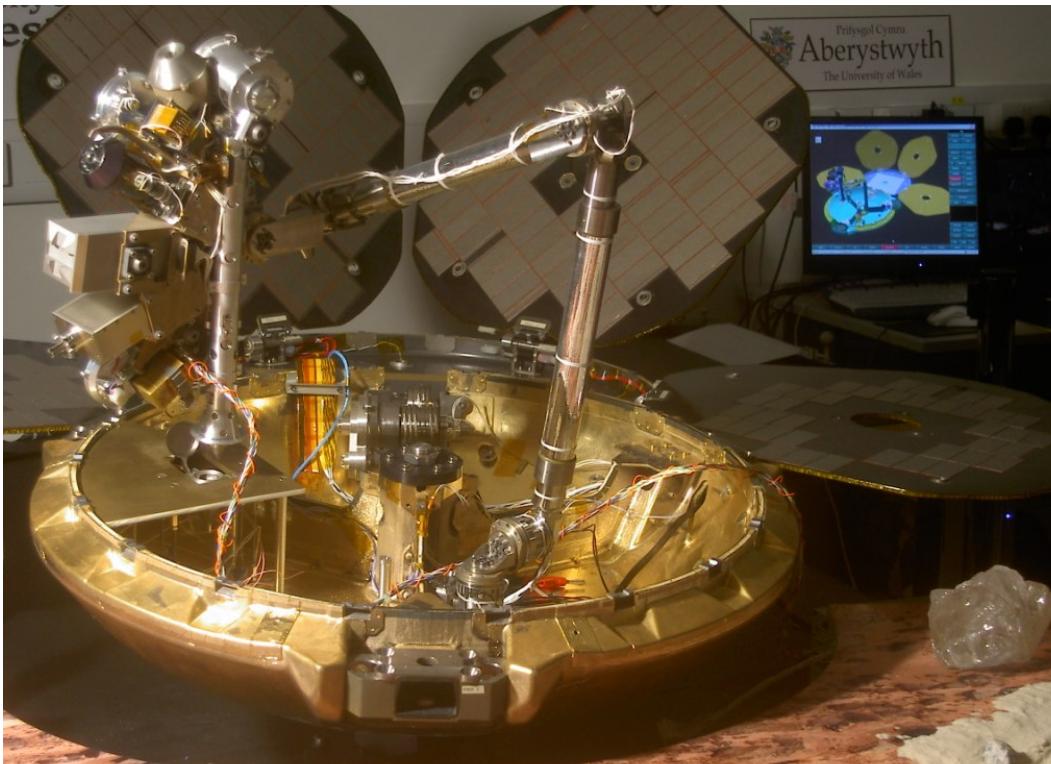
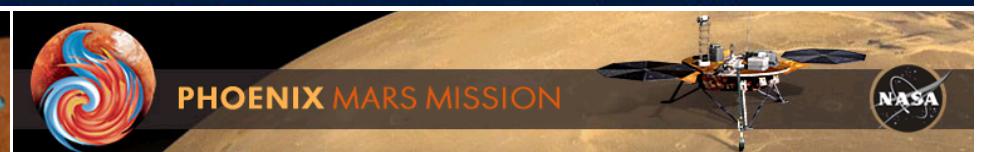
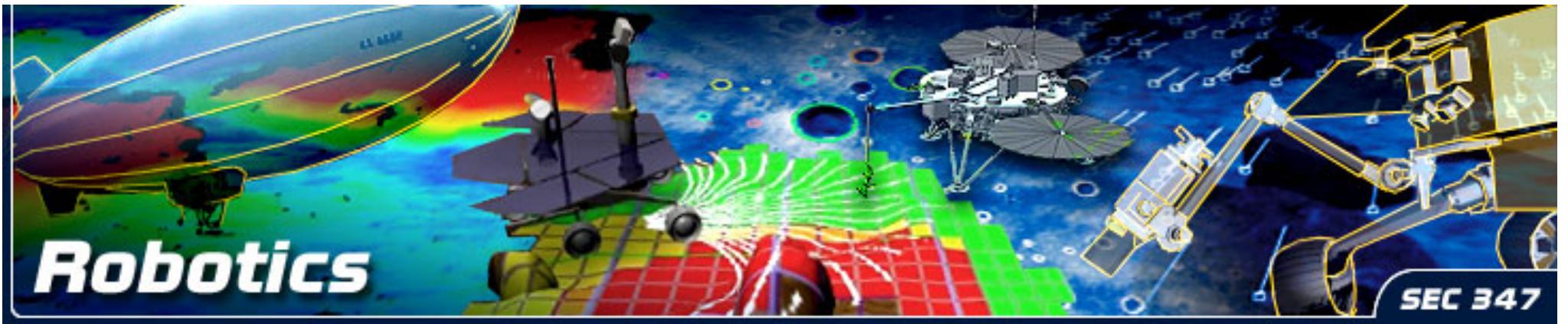
Robotický  
systém  
pro  
minilinvazivní  
chirurgii



ULTRAZVUKOVÉ SYSTÉMY VENTILAČNÍ TECHNIKA Toema

KARDIOLOGICKÉ A MONITOROVACÍ SYSTÉMY





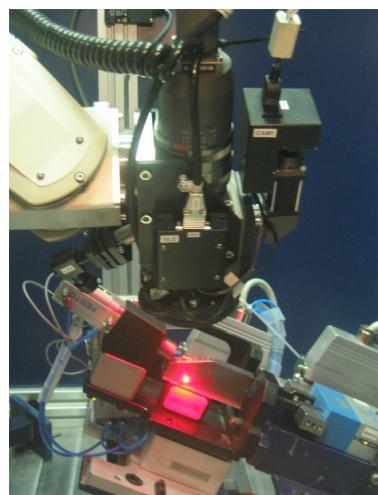
## Precision for industry



Low (e.g. manipulation)

$\pm 5$  mm in the whole working space  
 $\pm 0.5$  mm locally

... often available

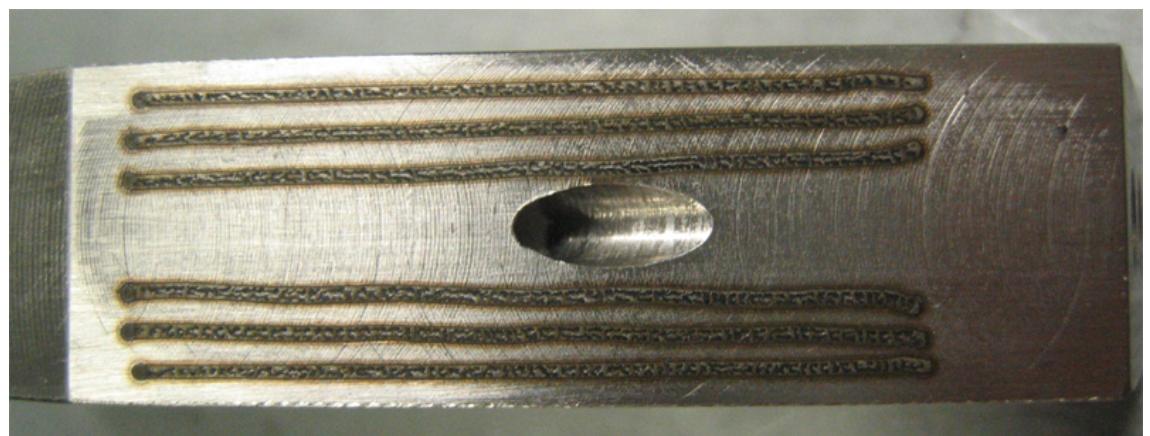
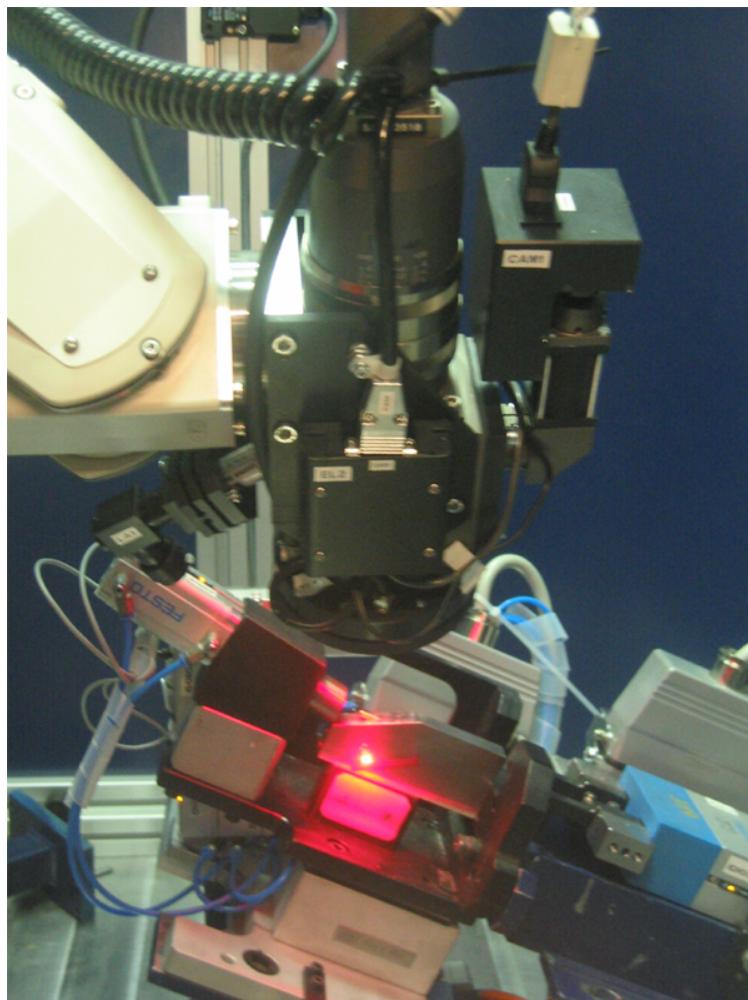


High (e.g. laser welding)

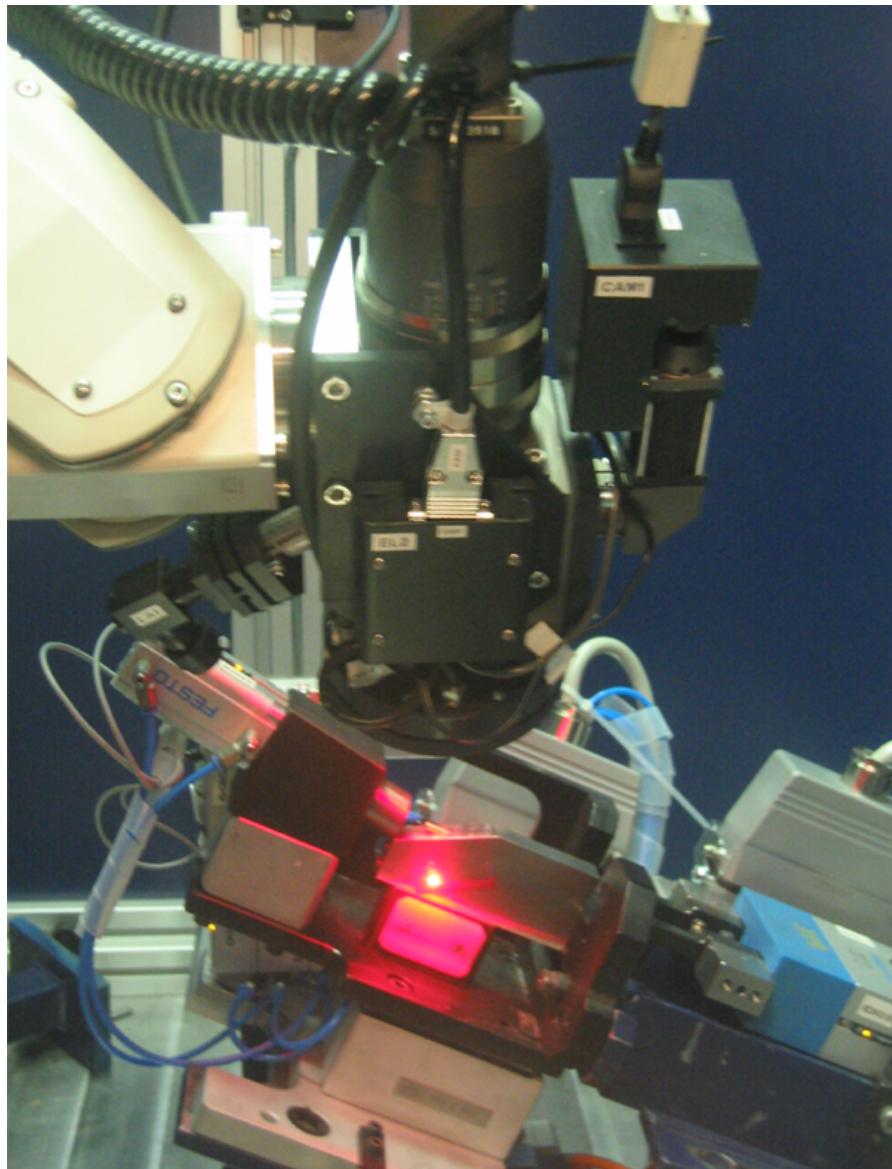
$\pm 0.5$  mm in the whole working space  
 $\pm 0.05$  mm locally

... often not available

Error  $\pm 0.5$  mm



## Modeling kinematics – calibration – absolute accuracy $\pm 0.05$ mm



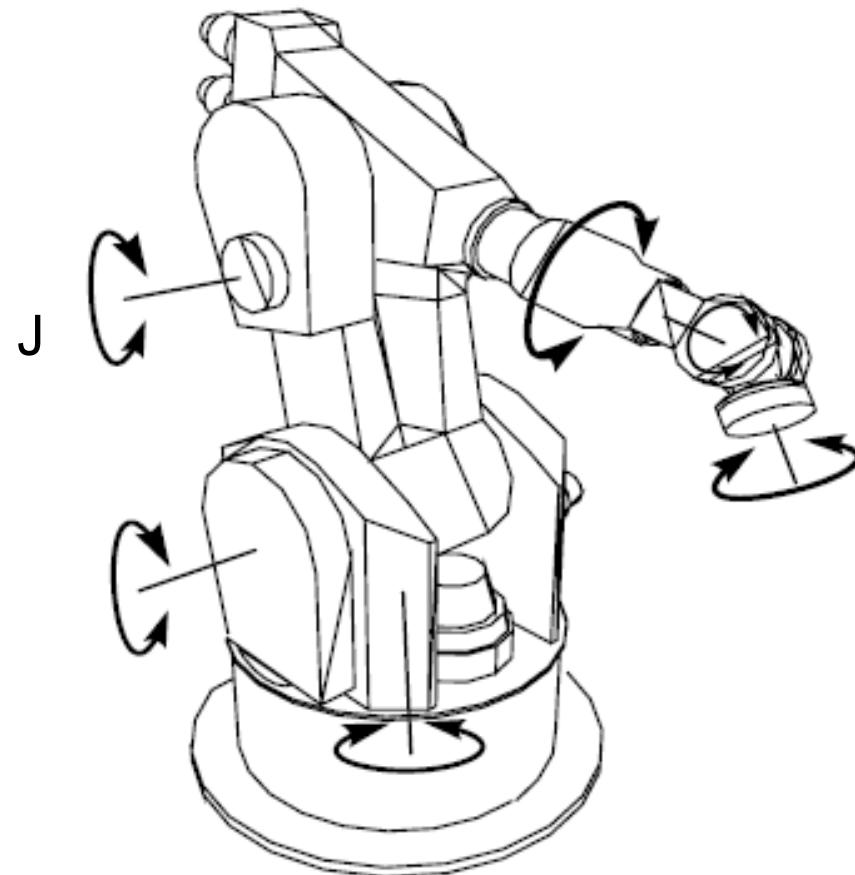
MITSUBISHI robot  
TRUMPF welding laser  
NEOVISION vision guiding

Robot-Vision calibration (courtesy Neovision s.r.o.)

## Two kinds of manipulators

1. Serial manipulators
2. Parallel manipulators

# Serial manipulators



KUKA manipulator

# Serial manipulators



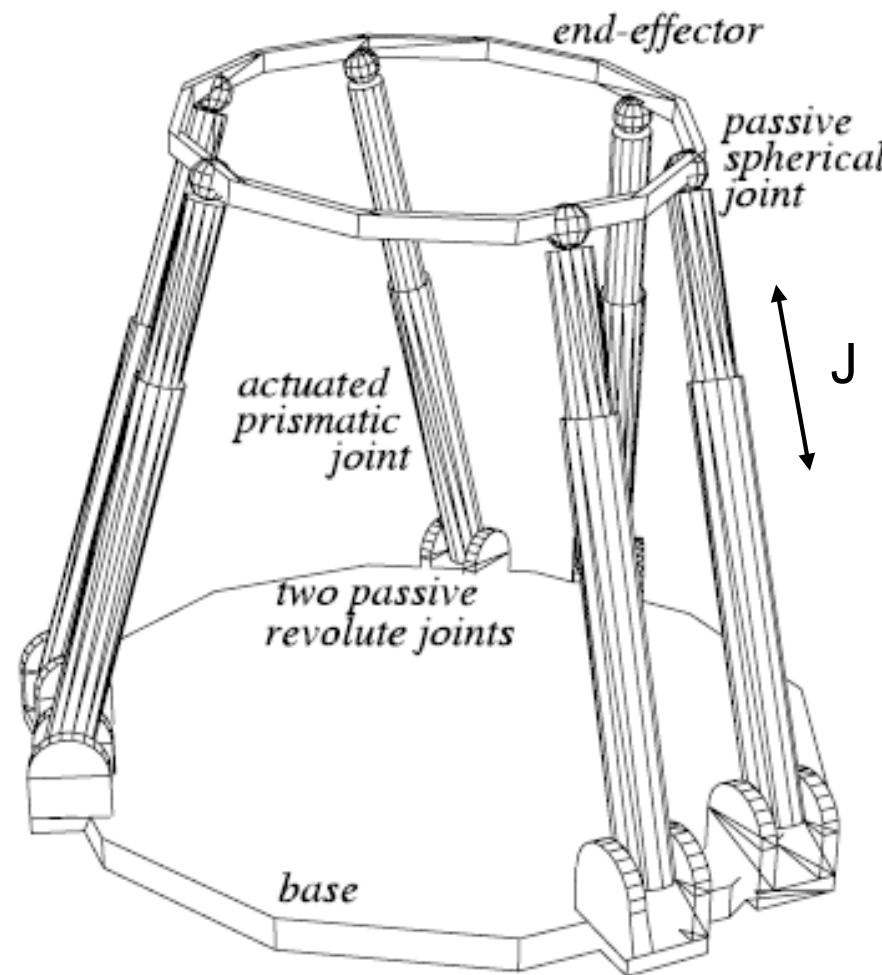
Stäubli (courtesy Neovision s.r.o.)



Mitsubishi (courtesy Neovision s.r.o.)

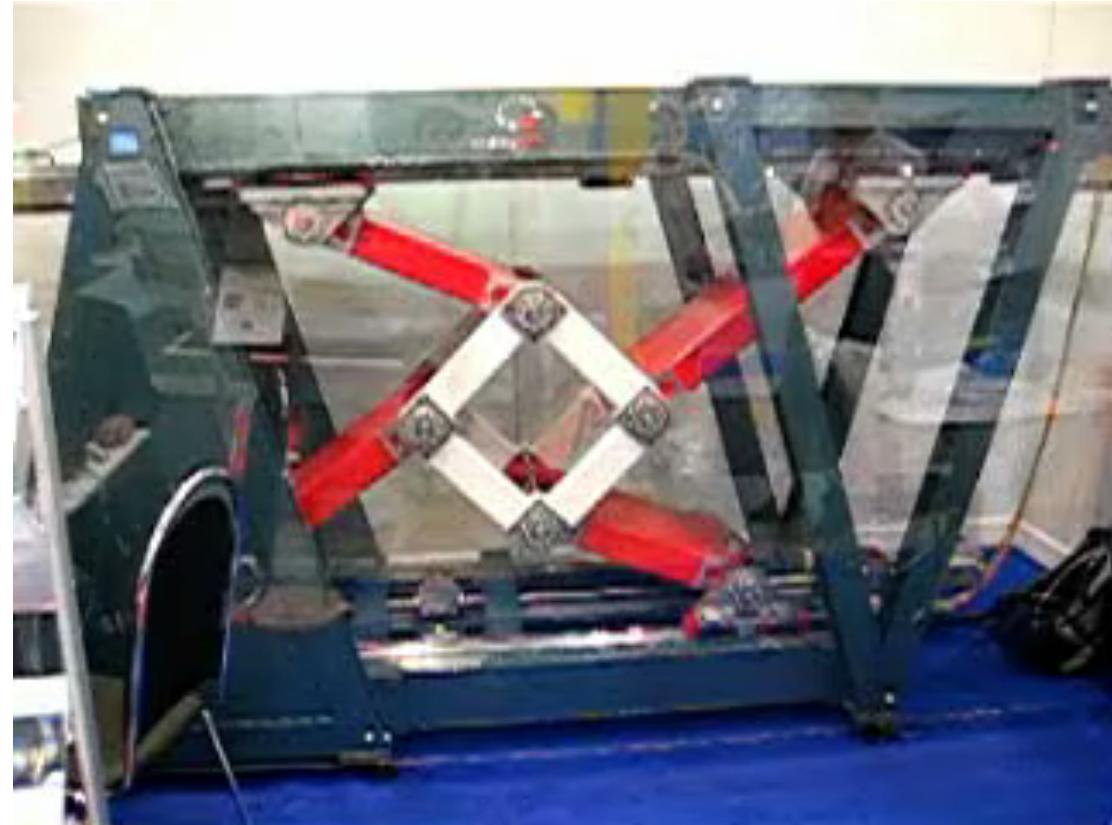
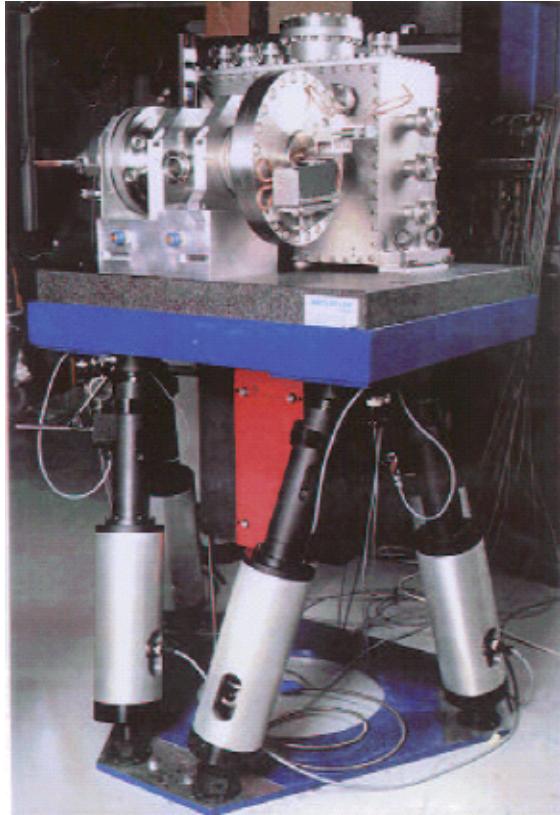
1. Direct kinematic task – easy
2. Inverse kinematic task – difficult

# Parallel manipulators



Stewart-Gough Platform

# Parallel manipulators



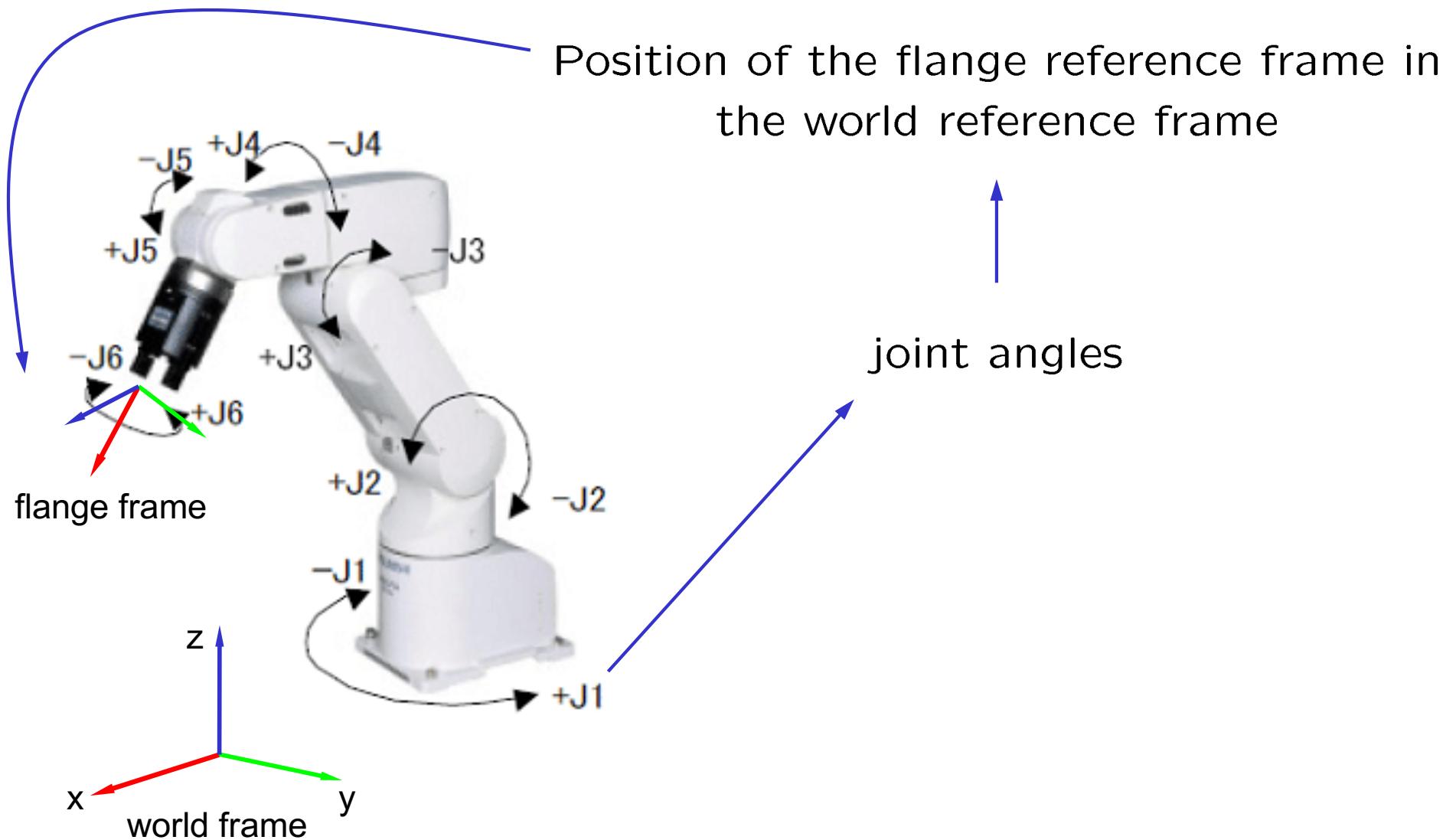
Sliding Star (courtesy of Prof. Valášek, CTU Prague)

1. Direct kinematic task – difficult
2. Inverse kinematic task – easy

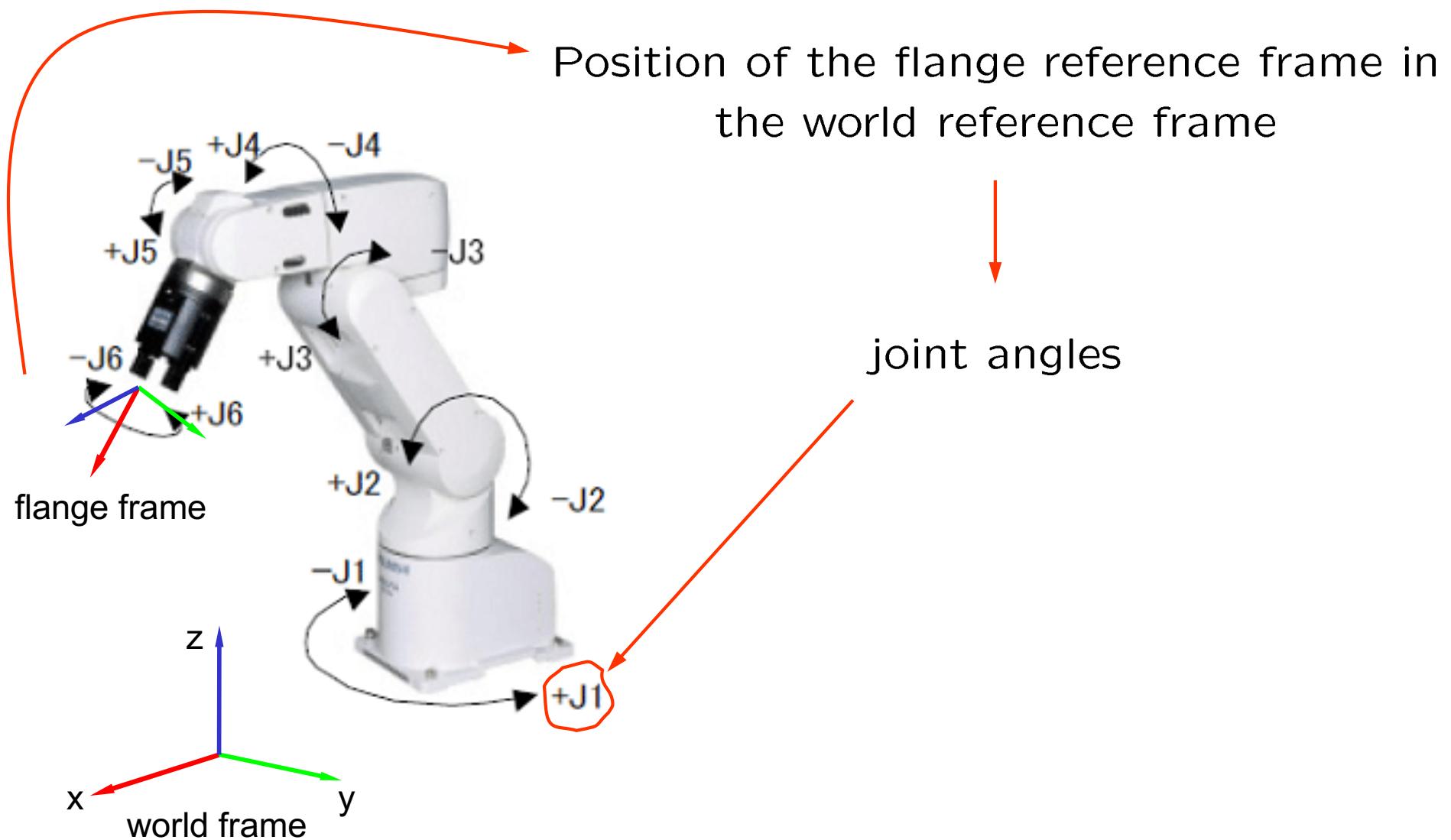
## Three main problems

1. Direct kinematic task (přímá kinematická úloha)
2. Inverse kinematic task (inverzní kinematická úloha)
3. Kinematic calibration (kalibrace kinematiky)

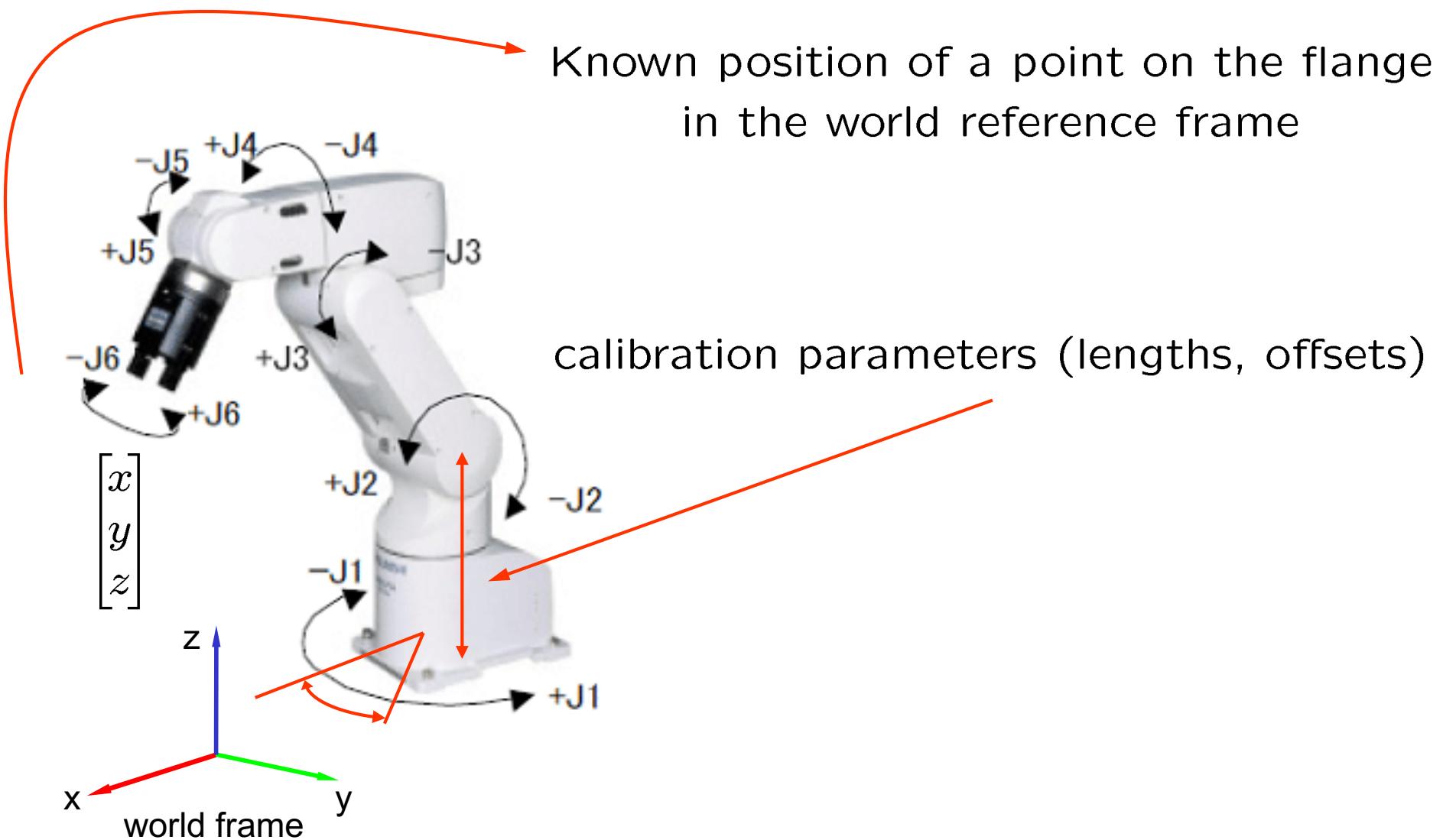
## Direct kinematic task



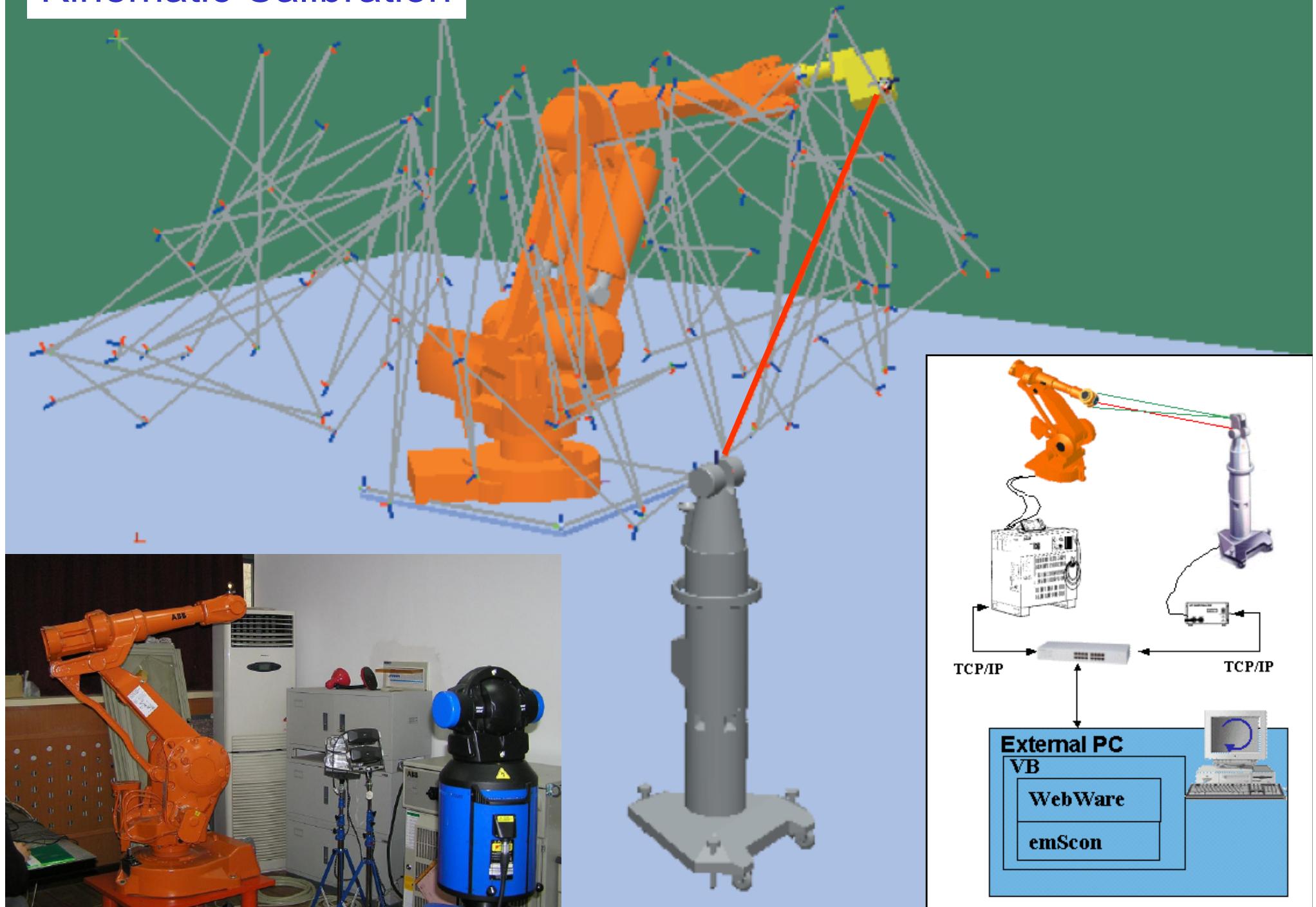
## Inverse kinematic task



## Kinematic calibration



# Kinematic Calibration

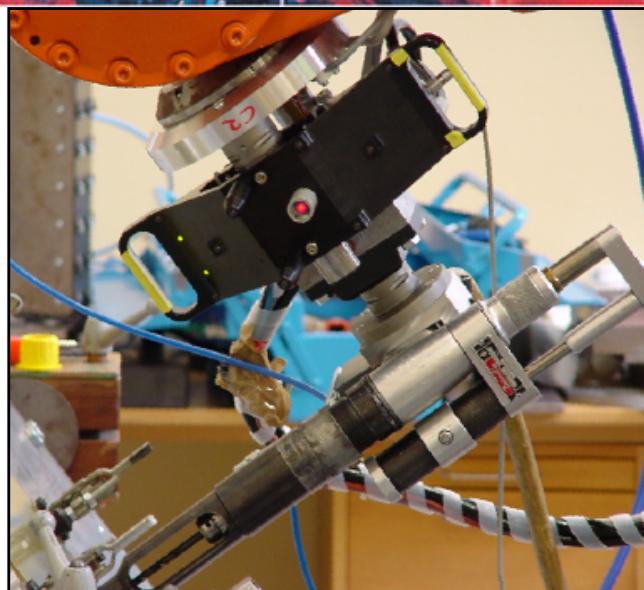
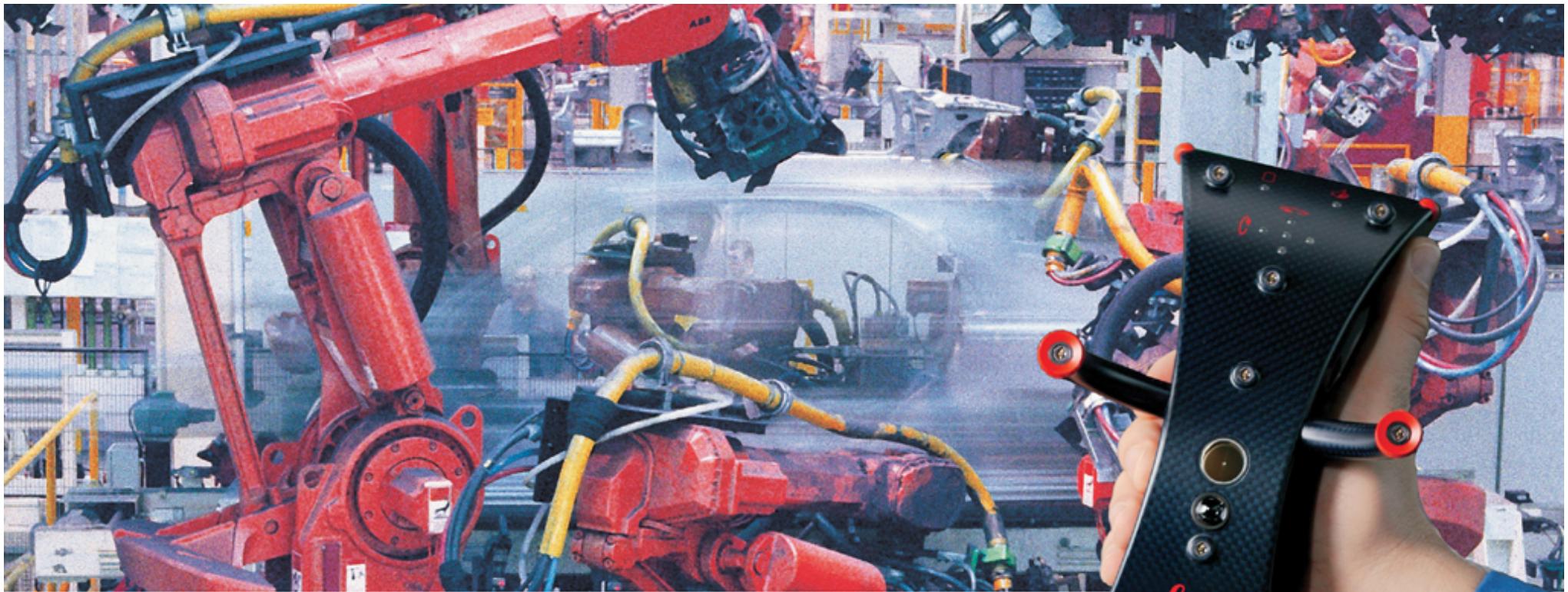


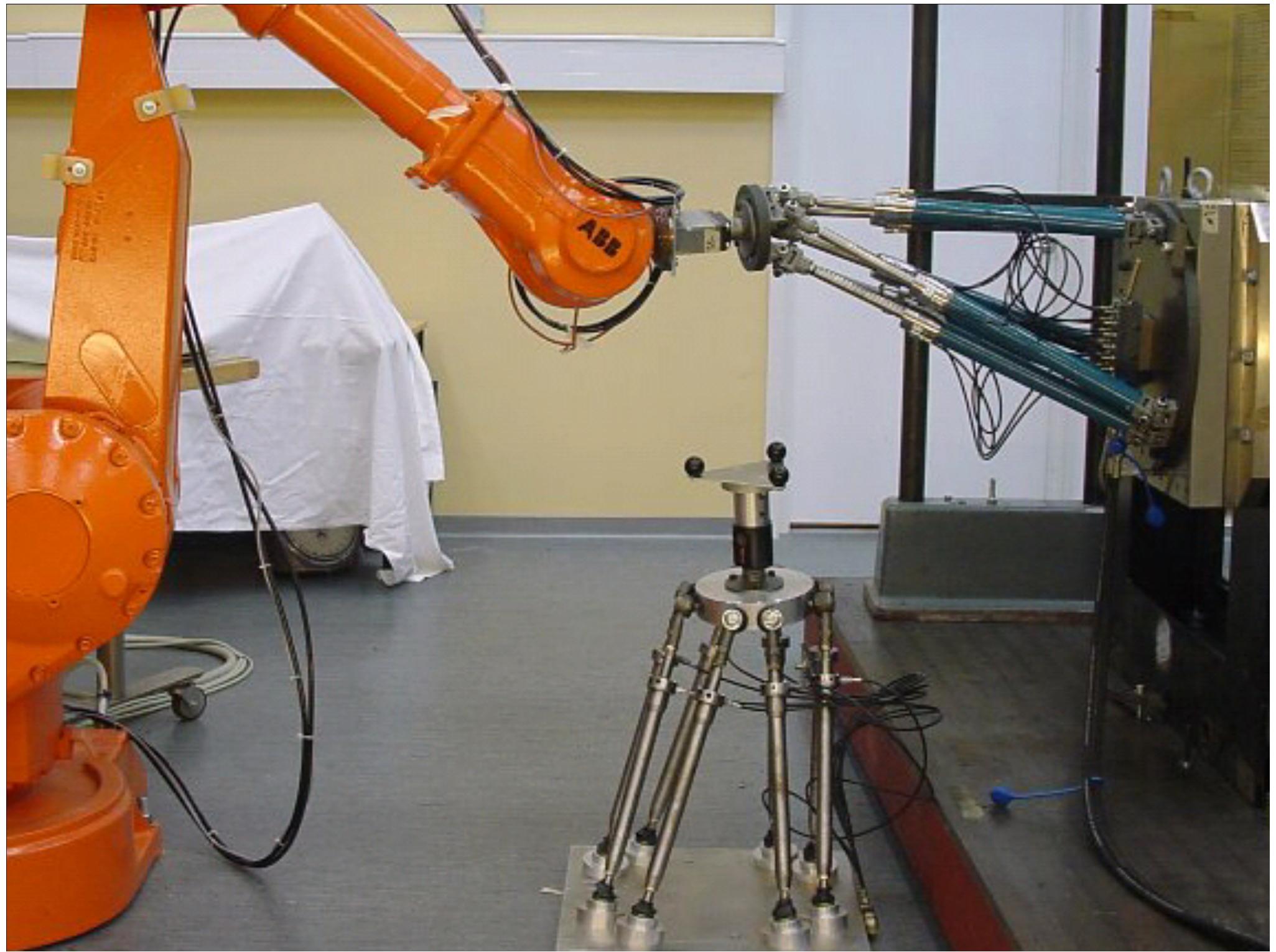
## Robot Calibration

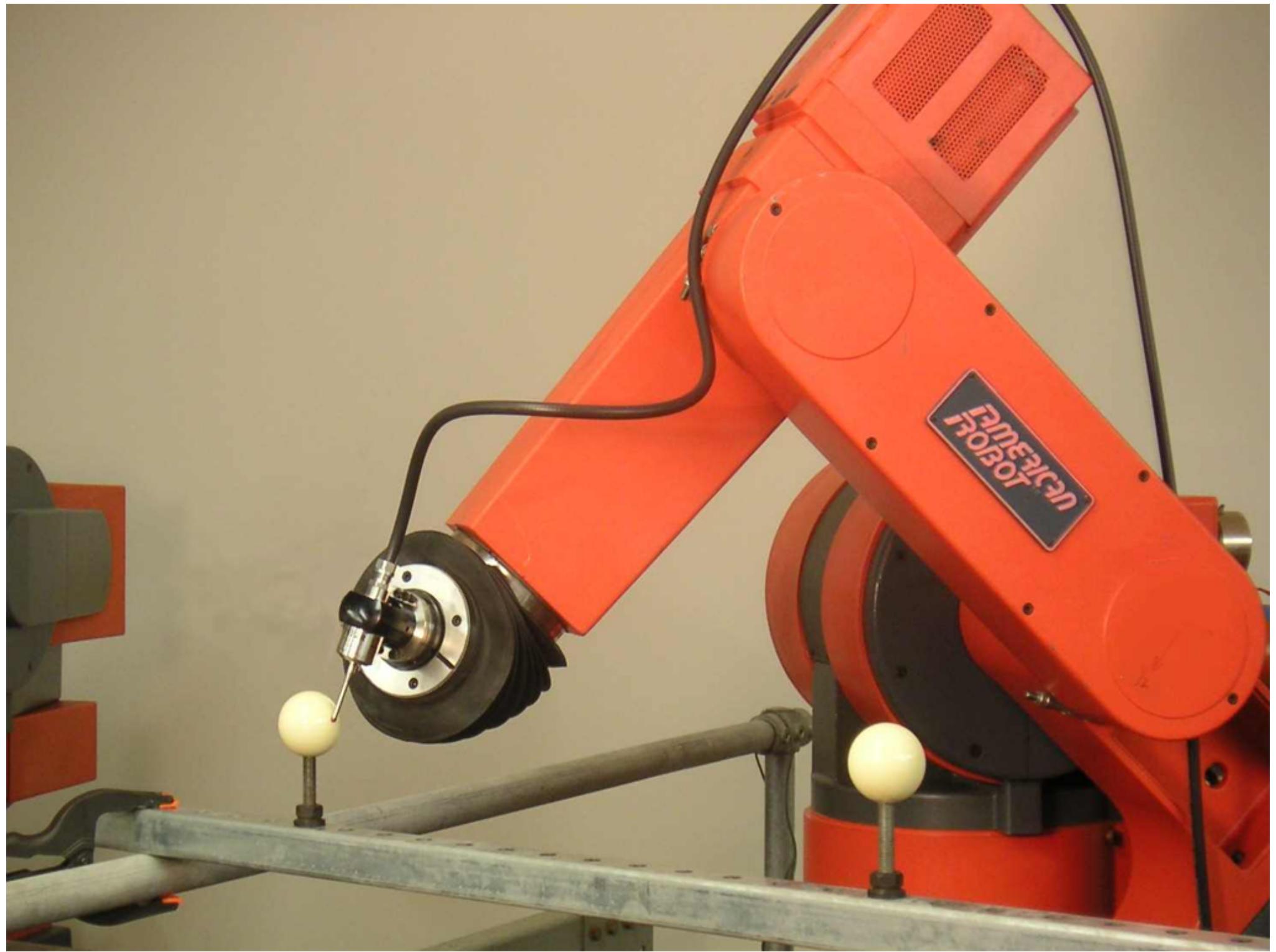


# Kinematic Calibration

**Leica**  
Geosystems

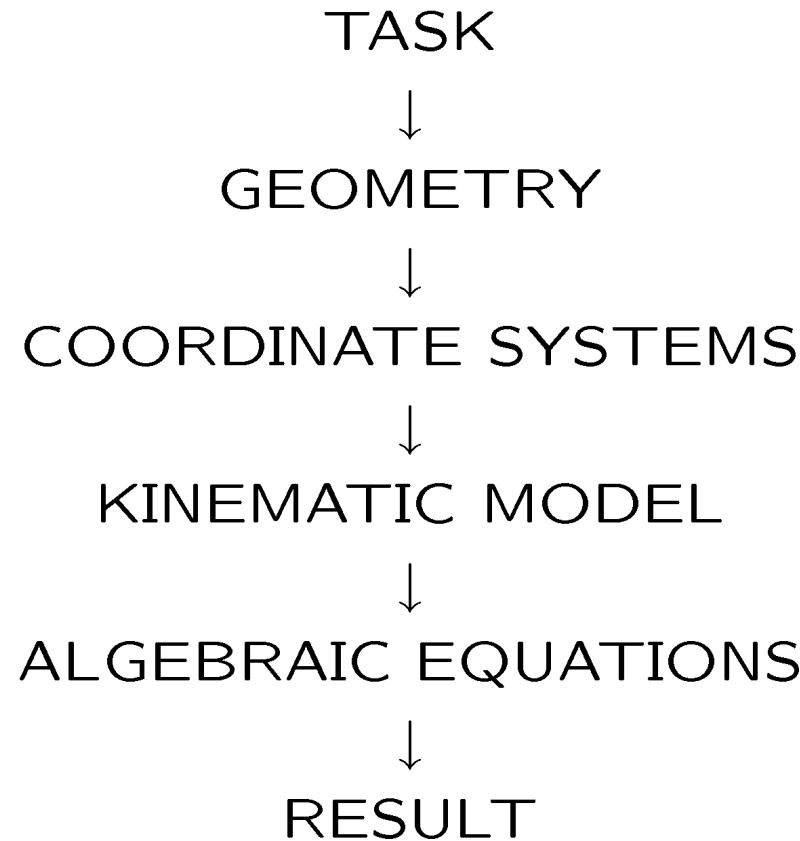








# Solving kinematic tasks



## Solving kinematic tasks

1968 Donald L. Pieper (Ph.D. thesis)

The inverse kinematics of any serial manipulator with six revolute joints, and with three consecutive joints intersecting, can be solved in closed-form, i.e., analytically.

1989 M. Raghavan, B. Roth. *Kinematic Analysis of the 6R Manipulator of General Geometry*. Int. Symp. Robotics. Research. Pp. 314-320, Tokyo 1989/1990.

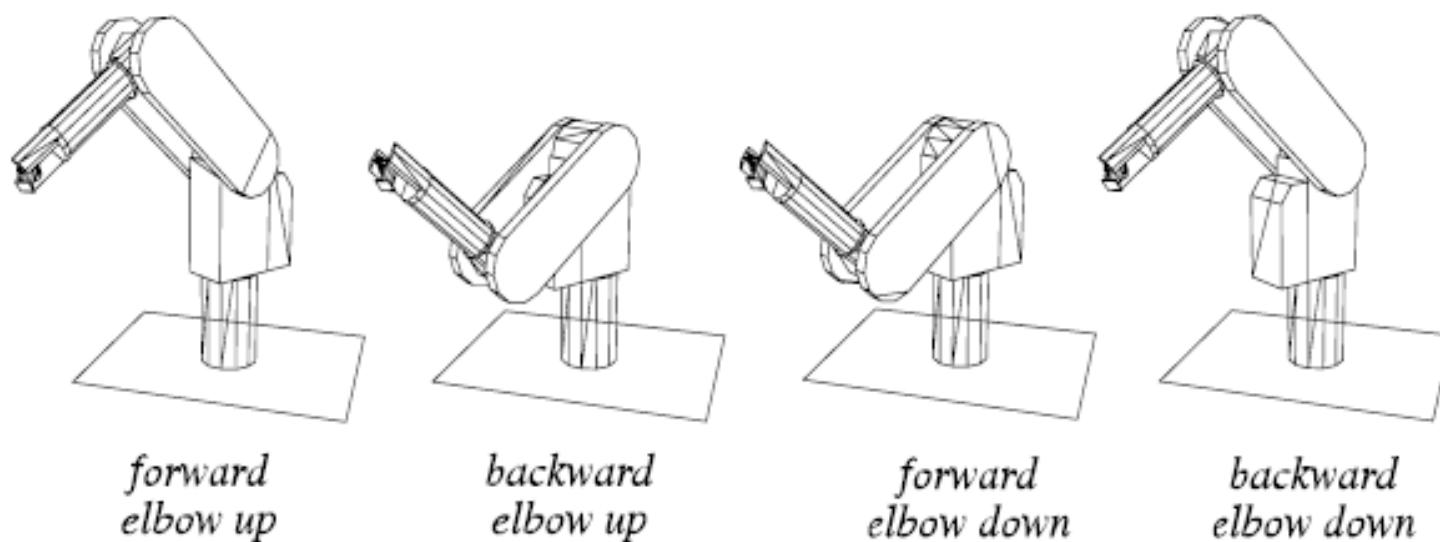
A general technique for computing inverse kinematics for any serial manipulator with six revolute joints.

... leads to solving an algebraic equation of degree 16.

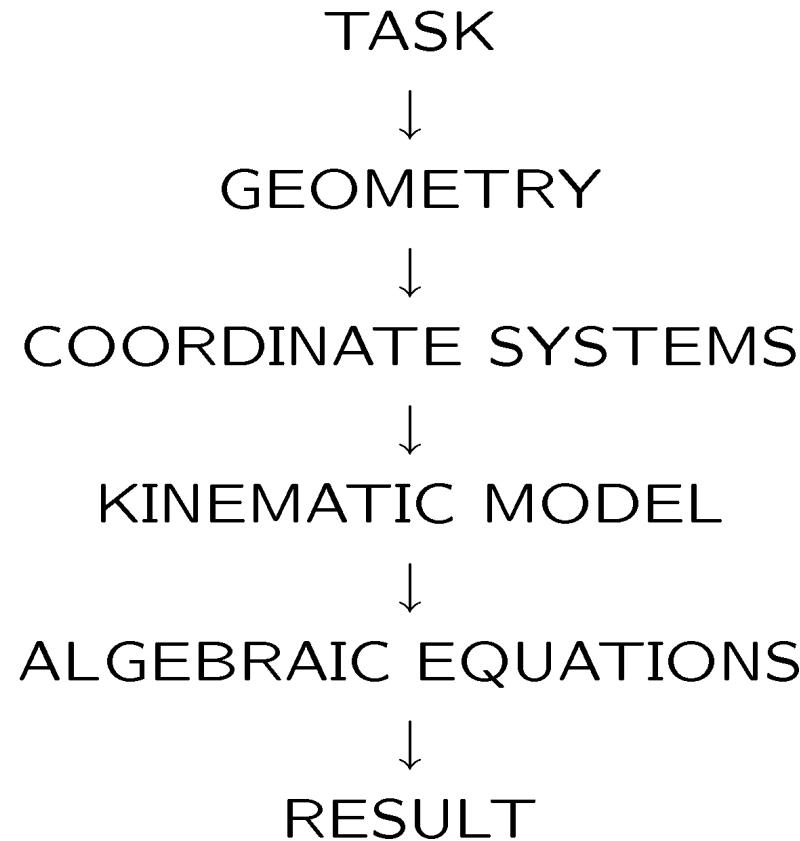
# Solving kinematic tasks

Algebraic equation of degree 16 ... up to 16 solutions

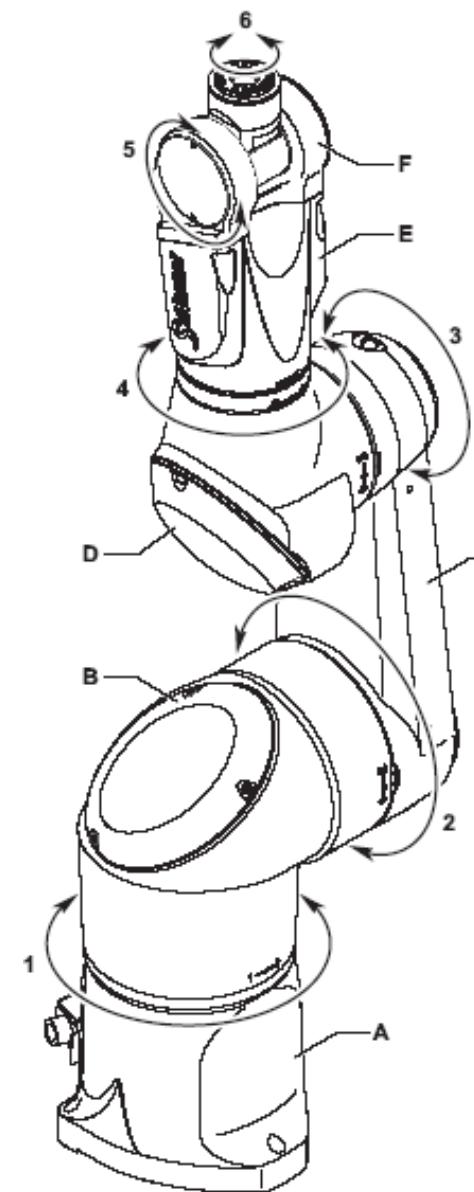
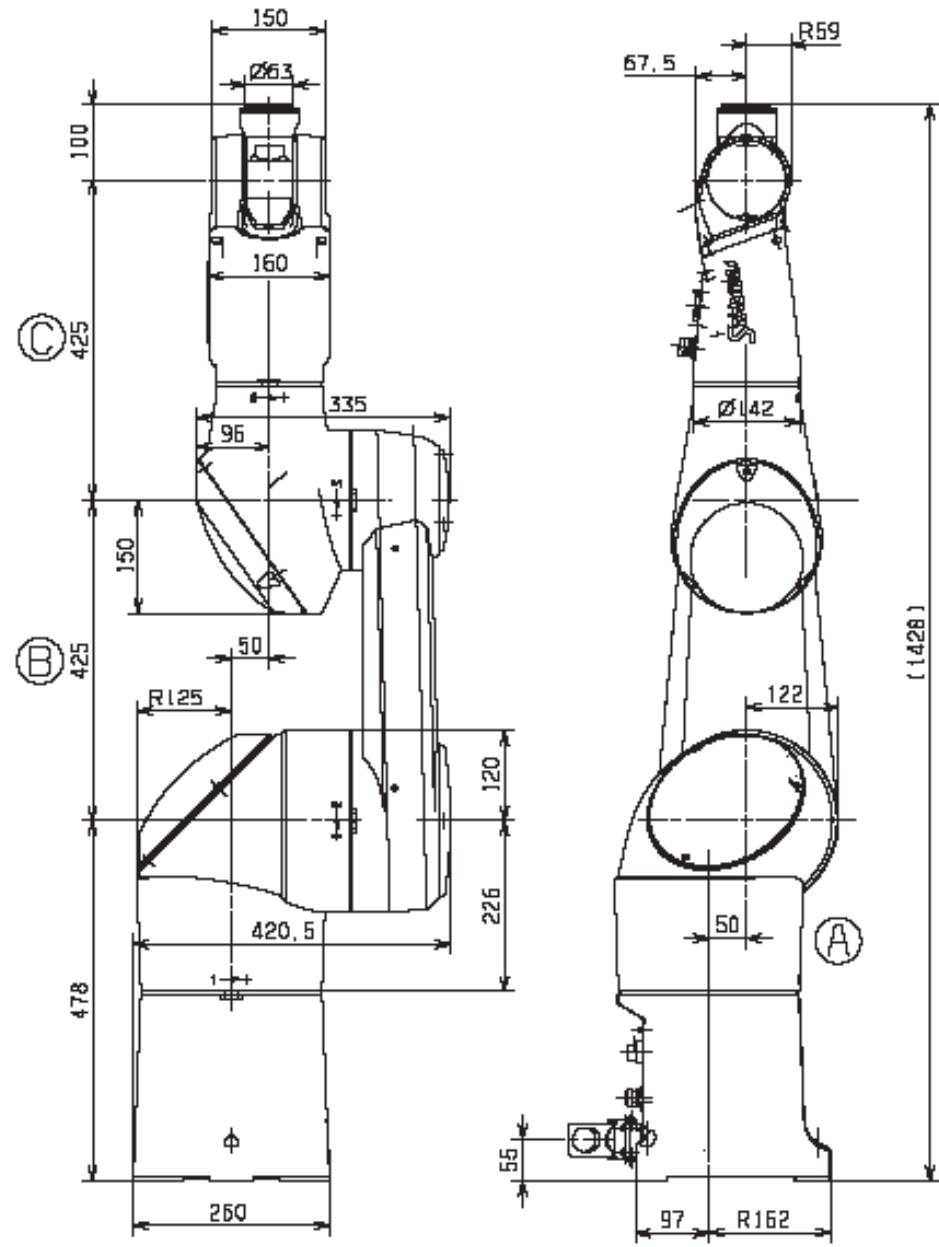
4 typical solutions



# Solving kinematic tasks

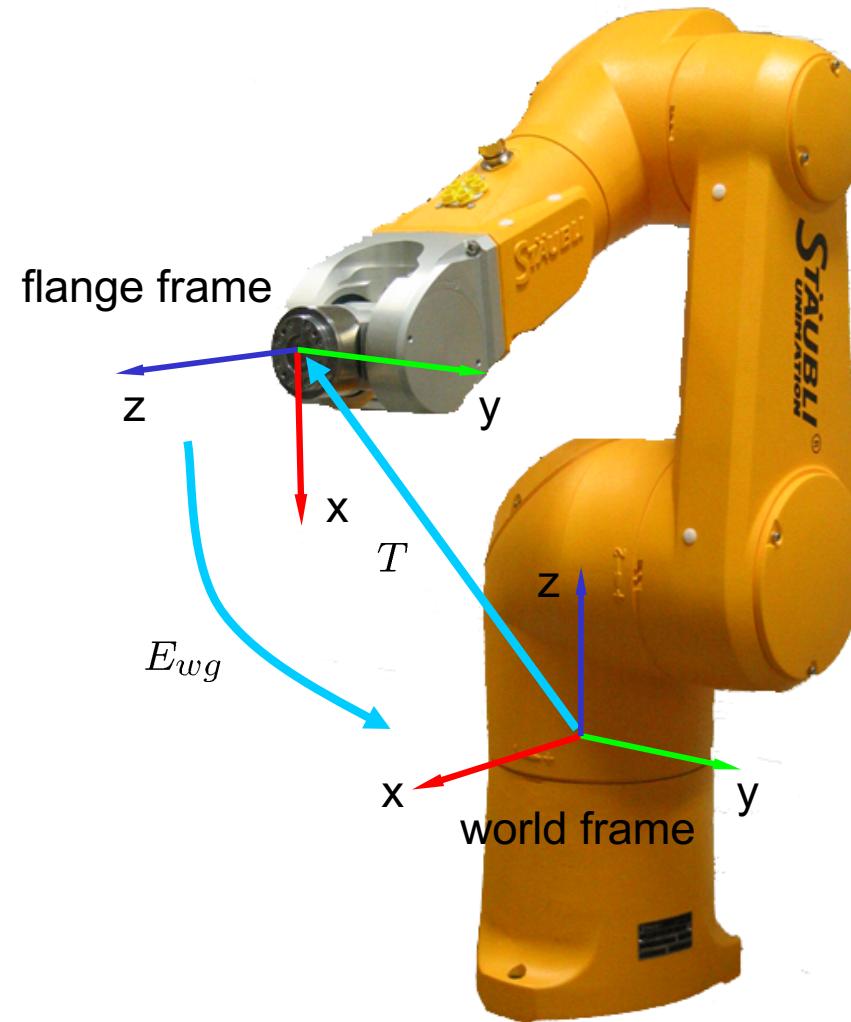


# Stäubli TX-90 – Geometry



**Figure 1.3 - Standard arm**

## Kinematic model

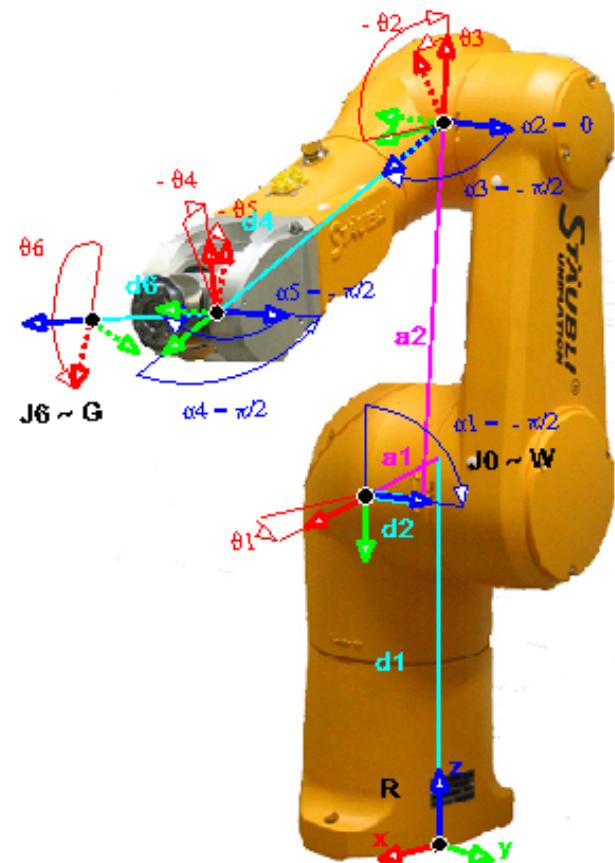


$$\alpha_i \mid a_i \mid \theta_i \mid d_i$$

$$A_i^{i-1} = \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cos \alpha_i & \sin \theta_i \sin \alpha_i & a_i \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cos \alpha_i & -\cos \theta_i \sin \alpha_i & a_i \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$G = A_1^0 A_2^1 A_3^2 A_4^3 A_5^4 A_6^5$$

$$A_1^0 = \begin{bmatrix} \cos \theta_1 & 0 & -\sin \theta_1 & a_1 \cos \theta_1 \\ \sin \theta_1 & 0 & \cos \theta_1 & a_1 \sin \theta_1 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



$$\text{offset} = [0, -\frac{\pi}{2}, -\frac{\pi}{2}, 0, 0, -\pi]$$

$$\begin{array}{c|c|c|c} \alpha_1 & a_1 & \theta_1 & d_1 \\ \hline -\frac{\pi}{2} & a_1 & \theta_1 & 0 \end{array}$$

$$\begin{array}{c|c|c|c} \alpha_2 & a_2 & \theta_2 & d_2 \\ \hline 0 & a_2 & \theta_2 & d_2 \end{array}$$

$$A_2^1 = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & a_2 \cos \theta_2 \\ \sin \theta_2 & \cos \theta_2 & 0 & a_2 \sin \theta_2 \\ 0 & 0 & 1 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{array}{c|c|c|c} \alpha_3 & a_3 & \theta_3 & d_3 \\ \hline -\frac{\pi}{2} & 0 & \theta_3 & 0 \end{array}$$

$$A_3^2 = \begin{bmatrix} \cos \theta_3 & 0 & -\sin \theta_3 & 0 \\ \sin \theta_3 & 0 & \cos \theta_3 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{array}{c|c|c|c} \alpha_4 & a_4 & \theta_4 & d_4 \\ \hline \frac{\pi}{2} & 0 & \theta_4 & d_4 \end{array}$$

$$A_4^3 = \begin{bmatrix} \cos \theta_4 & 0 & \sin \theta_4 & 0 \\ \sin \theta_4 & 0 & -\cos \theta_4 & 0 \\ 0 & 1 & 0 & d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{array}{c|c|c|c} \alpha_5 & a_5 & \theta_5 & d_5 \\ \hline -\frac{\pi}{2} & 0 & \theta_5 & 0 \end{array}$$

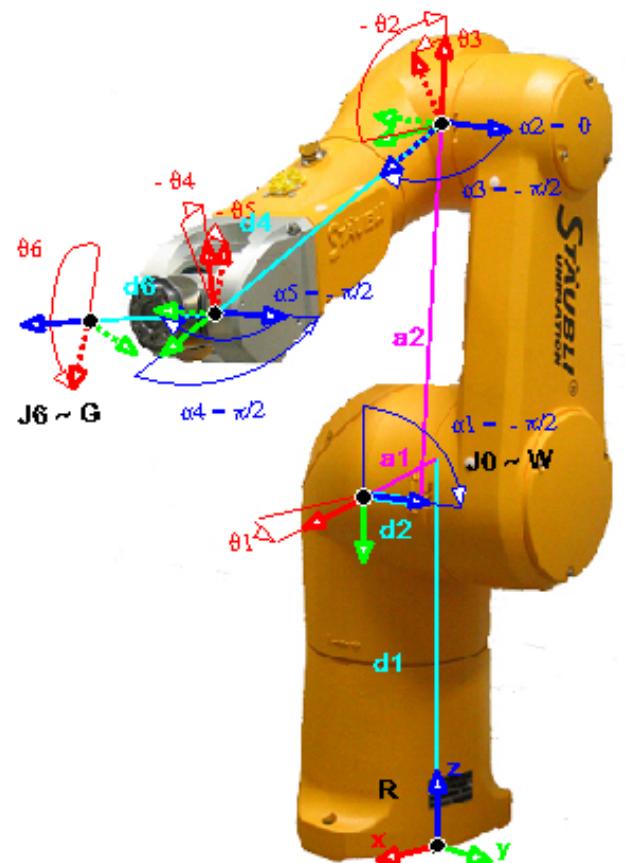
$$A_5^4 = \begin{bmatrix} \cos \theta_5 & 0 & -\sin \theta_5 & 0 \\ \sin \theta_5 & 0 & \cos \theta_5 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{array}{c|c|c|c} \alpha_6 & a_6 & \theta_6 & d_6 \\ \hline 0 & 0 & \theta_6 & d_6 \end{array}$$

$$A_6^5 = \begin{bmatrix} \cos \theta_6 & -\sin \theta_6 & 0 & 0 \\ \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# The Standard Kinematic model in Denavit-Hartenberg Convention

Stäubli TX 90



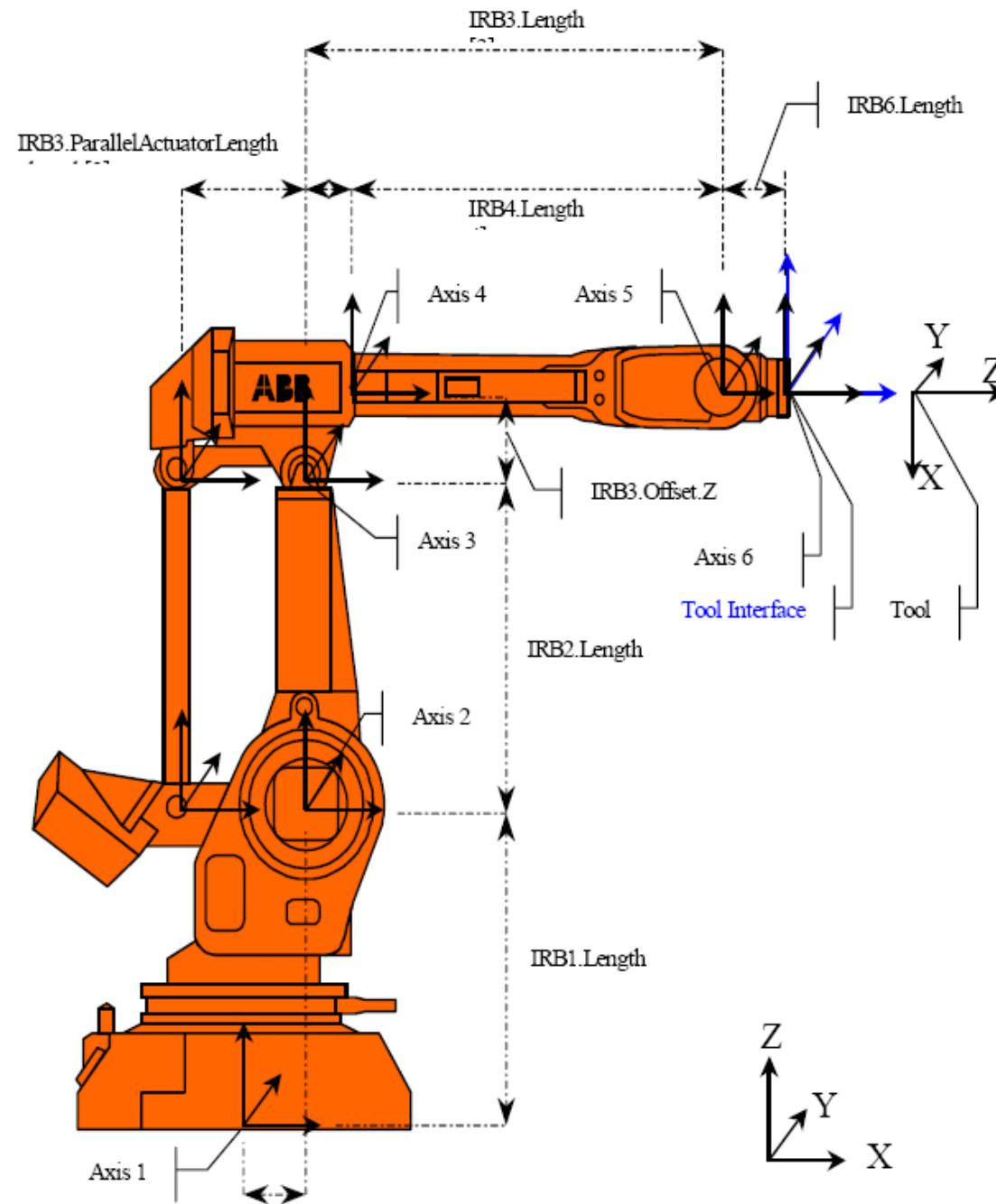
TX-90 (6 axis, RRRRRR) [Staubli]

$\alpha$	$a$	$\theta$	$d$
-1.5708	50.0	0.0	350.0
0.0	425.0	0.0	50.0
-1.5708	0.0	0.0	0.0
1.5708	0.0	0.0	425.0
-1.5708	0.0	0.0	0.0
0.0	0.0	0.0	100.0

6 non-trivial parameteres

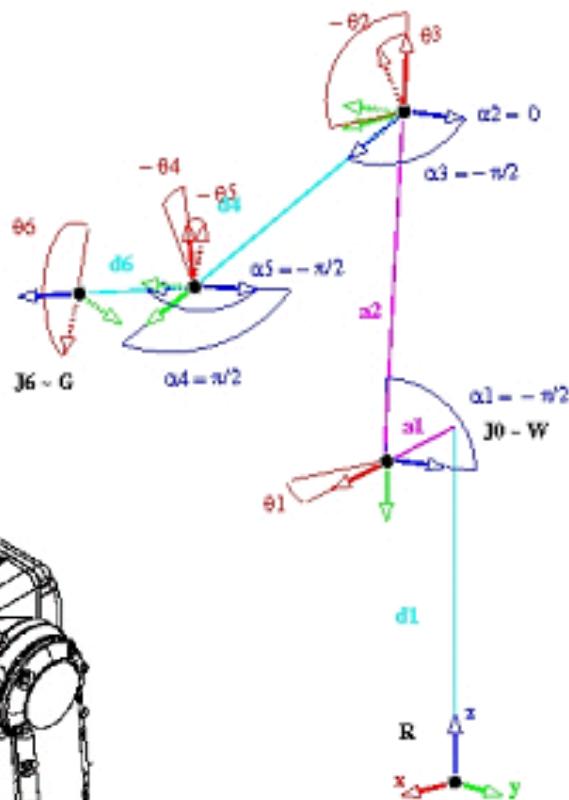
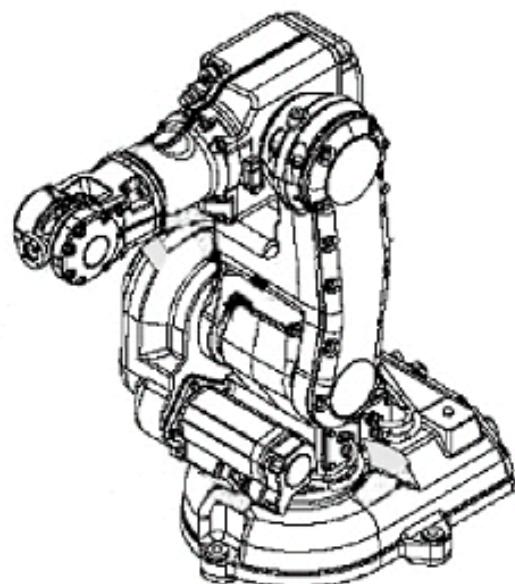
# The Standard Kinematic model in Denavit-Hartenberg Convention

ABB IRB 140



# The Standard Kinematic model in Denavit-Hartenberg Convention

ABB IRB 140



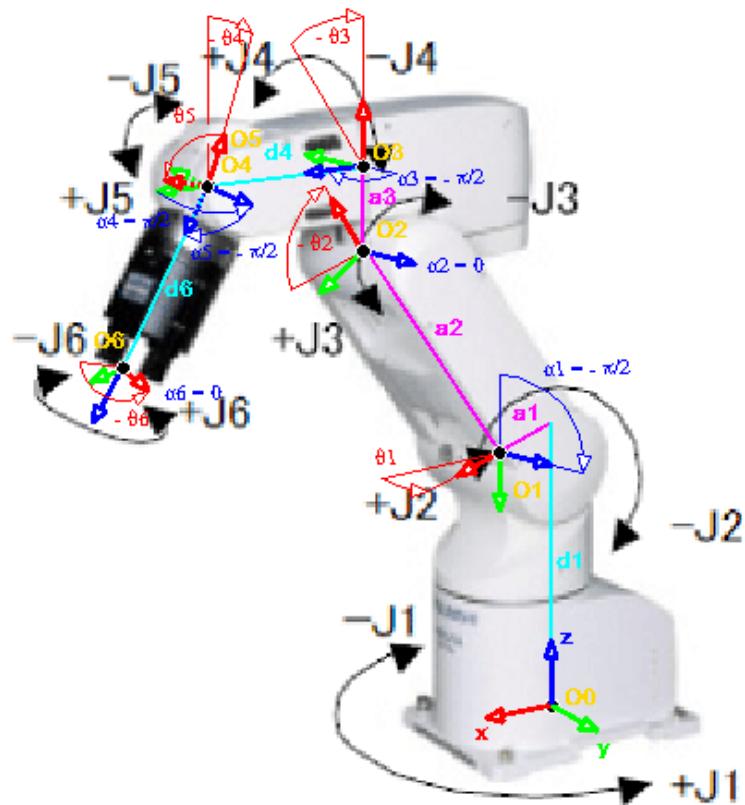
**IBR-140 (6 axis) [ABB]**

$\alpha$	$a$	$\theta$	$d$
-1.5708	70.0	0.0	352.0
0.0	360.0	0.0	0.0
-1.5708	0.0	0.0	0.0
1.5708	0.0	0.0	380.0
-1.5708	0.0	0.0	0.0
0.0	0.0	0.0	65.0

5 non-trivial parameteres

# The Standard Kinematic model in Denavit-Hartenberg Convention

Stäubli TX 90



**RV-6S (6 axis, RRRRRR) [Mitsubishi]**

$\alpha$	$a$	$\theta$	$d$
-1.5708	85.0	0.0	350.0
0.0	280.0	0.0	0.0
-1.5708	100.0	0.0	0.0
1.5708	0.0	0.0	315.0
-1.5708	0.0	0.0	0.0
0.0	0.0	0.0	85.0

6 non-trivial parameteres

# Special versus General Mechanisms

Special

×

General

simple & tractable

complicated & hard

$\alpha$	$a$	$\theta$	$d$
-1.5708	70.0	-	352.0
0.0	360.0	-	0.0
-1.5708	0.0	-	0.0
1.5708	0.0	-	380.0
-1.5708	0.0	-	0.0
0.0	0.0	-	65.0

$\alpha$	$a$	$\theta$	$d$
-1.42	70.1	- (+0.2)	352.0
0.10	360.0	- (+0.1)	0.2
-1.57	0.2	- (- 0.3)	0.3
1.58	0.1	- (+0.1)	380.2
-1.59	0.4	- (- 0.1)	0.1
0.07	0.2	- (- 0.2)	65.1

6 non-trivial parameters

×

18 (+6) non-trivial parameters

High precision → Small misalignments important → General mechanisms

# Literature

## Linear algebra

P. Pták. *Introduction to Linear Algebra*. Vydavatelství ČVUT, Praha, 2006.

## Numerical linear algebra

E. Krajník. *Maticový počet*. Vydavatelství ČVUT, Praha, 2000.

## The solution

M. Raghavan, B. Roth. *Kinematic Analysis of the 6R Manipulator of General Geometry*. Int. Symp. Robotics. Research. Pp. 314-320, Tokyo 1989/1990.

## The numerical solution

D. Manocha, J. Canny. *Efficient Inverse Kinematics for General 6R Manipulators*. Robotics and Automation 1994.

## The pedagogical solution will be developed using

D. Cox, J. Little, D. O'Shea. *Ideals, Varieties, and Algorithms*. Springer 1998.

# Software

Matlab: [www.matworks.com](http://www.matworks.com)

Maple: [www.maplesoft.com](http://www.maplesoft.com)

One algebraic equation in one variable

# SOLVING 1 ALGEBRAIC EQUATION

1 equation, 1 variable → companion matrix → eigenvalues

$$f(x) = x^3 + 4x^2 + x - 6 = -6 + 1x + 4x^2 + 1x^3$$

$$M_x = \begin{bmatrix} 0 & 0 & 6 \\ 1 & 0 & -1 \\ 0 & 1 & -4 \end{bmatrix}$$

... a simple rule

```
>> e=eig(M_x)
```

$$e = \begin{bmatrix} 1 \\ -2 \\ -3 \end{bmatrix} \quad x_1 = 1, x_2 = -2, x_3 = -3$$

It works when eig works, i.e. order 100 in Matlab is often OK.

# SOLVING 1 ALGEBRAIC EQUATION

Linear mapping  $M \in \mathbb{R}^{n \times n}$

Eigenvalues  $Mx = \lambda x$

$$\Updownarrow$$

$$Mx - \lambda x = 0$$

$$\Updownarrow$$

$$Mx - \lambda Ix = 0$$

$$\Updownarrow$$

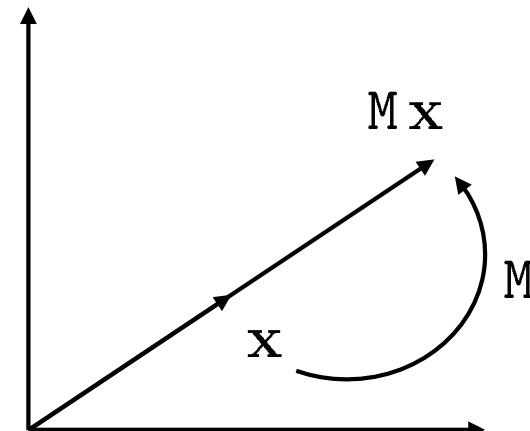
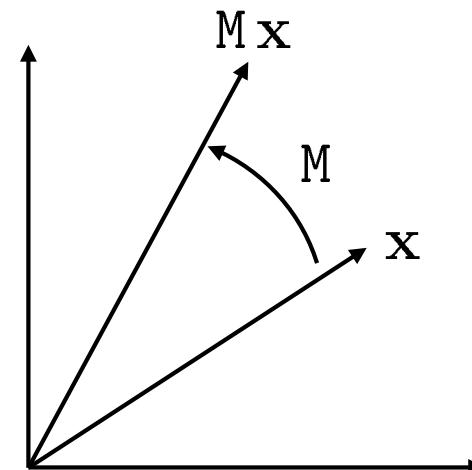
$$(M - \lambda I)x = 0$$

$$x \neq 0 \Rightarrow \Updownarrow$$

$$\text{rank}(M - \lambda I) < n$$

$$\Updownarrow$$

$$\det(M - \lambda I) = 0$$



# SOLVING 1 ALGEBRAIC EQUATION

algebraic equation

$$f(x) = x^4 + a_3 x^3 + a_2 x^2 + a_1 x + a_0 = \det(-M + x I)$$

$$-M + x I = \begin{bmatrix} \boxed{0} & & & a_0 \\ -1 & \boxed{0} & & a_1 \\ & -1 & \boxed{0} & a_2 \\ & & -1 & x + a_3 \end{bmatrix}$$

$$f(x) = x^4 + a_3 x^3 + a_2 x^2 + a_1 \boxed{x} + a_0$$

Numerical solution to  $f(x)$  is obtained by

```
>> x = eig(M);
```