# Computed Tomography (CT) Part 1

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# Radiation Types of Ionizing Radiation

Ionization



## Electromagnetic radiation



# X-rays for CT

- Electro-magnetic waves: no charge, no rest mass
- $\blacktriangleright$  Corresponding frequency range  $10^{15}~-10^{18}$  Hz
- Energies used in medical imaging are in the "hard X-ray" range
- Large penetration depth in light matrices (e.g. tissue)

# X-rays interaction with matter



#### Introduction to $\mathsf{CT}$

Hardware

Mathematics and Physics of CT

Radon transform

# Computed Tomography (CT) scanner



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# CT history

- **1917** mathematical theory (Radon)
- 1956 tomography reconstruction in radioastronomy (Bracewell)
- **1963** CT reconstruction theory (Cormack)
- **1971** CT principles demonstrated (Hounsfield)
- 1972 first working CT for humans (EMI, London, Hounsfield)
- 1973 PET, Positron Emission Tomography
- **1974** Ultrasound tomography
- **1975** whole body scanner (Hounsfield)
- 1982 Single Photon Emission Computed Tomography (SPECT)
- 1985 Helical CT
- 1998 Multislice CT, 0.5 s/frame

#### Johann Radon 1887–1956



D.J. Reisen

- born in Děčín (Czech Republic), lived in Göttingen, Brno, Hamburg, Greifswald, Erlangen, Breslau, Innsbruck and Vienna
- mathematician; Radon transform (1917) reconstruction of a function from its integrals on certain manifolds (projections)

# Godfrey Hounsfield



- physicist and engineer (did not attend university)
- worked on radar and on first transistor computers
- created the first CT X-ray scanner
- Nobel prize in Medicine (1979, together with Cormack)

# Allan MacLeod Cormack 1924–1998



- born in South Africa, studied in Cambridge, lived in the US
- particle physicist
- theoretical foundation of CT scanning (independently of Hounsfield)
- Nobel prize in Medicine (1979, together with Hounsfield)

# CT principles



1. Sequence of parallel sections (tomos)

# CT principles



- 1. Sequence of parallel sections (tomos)
- 2. Sequence of projections from multiple directions

# CT principles



- 1. Sequence of parallel sections (tomos)
- 2. Sequence of projections from multiple directions
- 3. Reconstruction of the object

### CT example scans



Head and kidneys

### CT example scans



CT angiography, pelvis





Lungs



LungsHead







LungsHead



- Lungs
- Head
- Abdomen



# Tomography modalities

- X-rays CT
- gamma rays PET, positron emission tomography
- gamma rays SPECT, single-photon emission computerized tomography
- light optical tomography
- RF waves MRI, magnetic resonance imaging
- DC electric impedance tomography
- ultrasound ultrasound tomography

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### First scanner



# Scanner geometry — generation 1



- Single source and single detector
- Finely collimated narrow beam
- Alternating translation and rotation
- Very slow (4 min / section), low resolution
- Low cost, good scatter rejection, easy calibration

# Scanner geometry — generation 2



- Narrow fan beam (~ 10°), multiple detectors (N)
- N projections acquired in parallel
- Increased rotation increment
- Increased speed (20 s / section)

Scanner geometry — generation 3 1975 Rotation only X - ray tube 30 Object WIIIIIII Detector or ray 3rd gen

- ▶ Wide fan beam  $(30^{\circ} \sim 60^{\circ})$  covering complete field of view
- 100s of detectors
- Only rotation, no translation
- Pulsed or continuous acquisition
- ► Fast (5 s / section)

Fan-beam detector



- Rotating source, stationary detector rings
- More expensive
- Avoids rotating contacts

Fast

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### Scanner geometry — generation 5 Electron beam CT (EBCT, 1983)



- No moving parts
- Directional X-ray source
- Extremely fast (beating heart)
- Lower signal to noise ratio and spatial resolution

# CT X-ray sources

Similar but bigger than radiography X-ray sources

Typical properties of an X-ray tube used for CT compared to those of a conventional radiographic tube.

	Conventional	
	X-Ray Tube	CT X-Ray Tube
Typical exposure parameters	70 kV, 40 mAs	120 kV, 10,000 mAs
Energy requirements	2,800 J	1,200,000 J
Anode diameter	100 mm	160 mm
Anode heat storage capacity	450,000 J	3,200,000 J
Maximum anode heat dissipation	120,000 J/min	540,000J/min
Maximum continuous power rating	450 W	4000 W
Cooling method	Fan	Circulating oil

Challenges: Power leads, cooling, vibration, ...

# CT X-ray sources

#### Similar but bigger than radiography X-ray sources



Challenges: Power leads, cooling, vibration, ...

# CT X-ray sources - novel approach

Liquid anode tube: overcoming power density limitations of solid target X-ray tubes



Liquid metal-jet tube:

- Heat dissipation problem nearly obsolete
- $\blacktriangleright\,$  Small focal sizes viable (10-15µm) at high power ( $\sim 500\,W)$ 
  - $\Rightarrow$  Allows for high magnification / system resolution

# Filtering and collimation (1)



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# Filtering and collimation (2)

Beam shaping (attenuate lateral part of the beam)



Pre-patient and detector collimation — beam(slice) width

# CT detector types

- Xenon ionization chamber detectors
  - Faster but less sensitive
- Scintillation detectors
  - More sensitive but slower (afterglow, scintillator dependent)



## CT detector types

	Xenon Detectors	Crystal Scintillator	Ceramic Scintillator
Detector	High pressure (8–25 atm) Xe ionisation chamber	CaWO <sub>4</sub> + silicon photodiode	Gd <sub>2</sub> O <sub>2</sub> S + silicon photodiode
Detector array	Single chamber, divided into elements by septa	Discrete detectors	Discrete detectors
Signal	Proportional to ionisation intensity	Proportional to light intensity	Proportional to light intensity
Detector efficiency	40%-70%	95%-100%	90%-100%
Geometric efficiency (in fan direction)	>90%	>80%	>80%
Afterglow limitations	No	Yes	No
Detector matching	No	Yes	Yes

#### Properties of detectors in common use in CT scanning.

#### Scintillation detector construction



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### Scintillation detector construction



Multiple (e.g. 32, 64) slices  $\longrightarrow$  acceleration



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# X-ray detectors: Photon counting detectors



- Unlimited dynamic range and exposure time
- Detected count obeys Poisson distribution

## Electric processing — corrections

- Offset correction (zero signal at rest)
- Normalization correction (x-ray source intensity fluctuation)
- Sensitivity correction (inhomogeneous detectors and amplifiers)
- Geometric correction
- Beam hardening correction
- Cosine correction (for fan beam geometry)

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#### Attenuation along a line



Homogeneous material (Beer-Lambert's law)

$$I = I_0 e^{-\mu \Delta \xi}$$

Piecewise homogeneous material

$$I = I_0 \prod_{i=1}^{n} e^{-\mu\Delta\xi} = I_0 e^{-\Delta\xi \sum_{i=1}^{n} \mu_i}$$

Continuously varying  $\mu(x)$ ,  $x = i\Delta\xi$ 

$$I = I_0 e^{-\lim_{\Delta \xi \to 0} \Delta \xi \sum_{i=1}^n \mu}$$
$$= I_0 e^{-\int_0^D \mu(x) dx}$$

Line integral for line L

$$= I_0 \mathrm{e}^{-\int_L \mu(\mathbf{x}) \mathrm{d}\mathbf{x}}$$

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# Hounsfield units

$$\mathcal{CT} = 1000 rac{\mu - \mu_{\mathsf{water}}}{\mu_{\mathsf{water}}}$$

- ▶ Values between −1000 (air) and approximately 1000 (bones)
- Densities in HU are reproducible between devices
- ► To differentiate soft tissue types, tumor types etc.
- Accurate calibration is needed

# Hounsfield units

HU, CT number



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Attenuation decreases with E



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- Attenuation decreases with E
- $\blacktriangleright$   $\longrightarrow$  low *E* rays are attenuated more
- $\blacktriangleright$   $\longrightarrow$  mean *E* increases
- Measured attenuation  $p = \log(I_0/I) <$  theoretically linear  $\mu \Delta \xi$ .

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- Beam hardening correction

### Attenuation, interaction of radiation with matter



"absorption edges" correspond binding energies of electrons from atom's shells.  $51\,/\,64$ 



high-Z candidate materials have been identified in recent years
Extensive pre-clinical testing and method development required

## Linear forward problem



For N straight lines  $L_j$ , measure the attenuation

$$p_j = \log rac{l_0^j}{l^j} = \int_{L_j} \mu(\mathbf{x}) \mathrm{d}\mathbf{x}$$

#### Assumptions

- Infinitely thin rays
- Straight lines no scattering, reflection or refraction
- Monochromatic radiation no beam hardening

(Assumptions can be relaxed but more complicated dependency.)

### Linear forward problem

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#### Assumptions

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(Assumptions can be relaxed but more complicated dependency.) **Discretization** 

$$\mu(\mathbf{x}) = \sum_{i=1}^{M} c_i \psi_i(\mathbf{x})$$

 $\longrightarrow$  linear system of equations  $L \boldsymbol{c} = \boldsymbol{p}$ 

### Integration lines in polar coordinates



Describe integration lines by angle  $\varphi$  and offset r:

$$L(\varphi, r) = \{ (x, y) \in \mathbb{R}^2; x \cos \varphi + y \sin \varphi = r \} \\ = \{ (r \cos \varphi - t \sin \varphi, r \sin \varphi + t \cos \varphi); t \in \mathbb{R} \}$$

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#### Integration lines in polar coordinates

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Implicit line equation,  $\mathbf{x} = (x, y)$ 

$$[\cos \varphi, \ \sin \varphi] \mathbf{x} = \mathbf{0}$$

Parametric line equation

$$\underbrace{\begin{bmatrix} \cos\varphi & -\sin\varphi \\ \sin\varphi & \cos\varphi \end{bmatrix}}_{\text{rotation matrix } R(\varphi)} \begin{bmatrix} r \\ t \end{bmatrix} = \mathbf{x}$$

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Rotating system of coordinates

$$\begin{bmatrix} \xi \\ \eta \end{bmatrix} = R(\varphi) \begin{bmatrix} \xi' \\ \eta' \end{bmatrix}$$
$$\begin{bmatrix} \xi' \\ \eta' \end{bmatrix} = R^{T}(\varphi) \begin{bmatrix} \xi \\ \eta \end{bmatrix}$$
$$R^{T}(\varphi) = R(-\varphi)$$

Projection

$$\mathsf{P}_arphi(\xi') = \int_{L(arphi,\eta')} \mu(\mathbf{x}) \mathrm{d}\mathbf{x} = \int o(\xi,\eta') \mathrm{d}\eta'$$

Measurements

$$P_{arphi}(\xi') = \log rac{I_0}{I(arphi,\xi')}$$



Change of variables

$$\xi' = r, \quad \eta' = t, \quad x = \xi, \quad y = \eta$$

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#### Radon transform

Projection in polar coordinates:

$$egin{aligned} & P_{arphi}(\xi') = \mathscr{R}[o(\xi,\eta)] \ & P_{arphi}(\xi') = \int_L o(\xi,\eta) \mathrm{d}t \end{aligned}$$

along the line L defined by  $\varphi$  a  $\xi'$ :

$$\xi' = \xi \cos \varphi + \eta \sin \varphi$$

Equivalently

$$P_{arphi}(\xi') = \int o(\xi' \cos arphi - \eta' \sin arphi, \xi' \sin arphi + \eta' \cos arphi) \mathrm{d} \eta'$$

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#### Radon transform properties

Motivation: If a function f represents an unknown density, then the Radon transform represents the projection data obtained as the output of a tomographic scan. Hence the inverse of the Radon transform can be used to reconstruct the original density from the projection data, and thus it forms the mathematical background for tomographic reconstruction.

Linearity:

$$\mathscr{R}[\alpha f + \beta g] = \alpha \mathscr{R}[f] + \beta \mathscr{R}[f]$$

Periodicity:

$$P_{arphi}(\xi') = P_{arphi \pm 2\pi}(\xi') = P_{arphi \pm \pi}(-\xi')$$

... and many others

#### Radon transform of a point

$$\begin{split} o(\xi,\eta) &= \delta(\xi - \xi_0, \eta - \eta_0) \\ P_{\varphi}(\xi') &= \mathscr{R}\big[o(\xi,\eta)\big] = \delta\big(\xi_0 \cos \varphi + \eta_0 \sin \varphi - \xi'\big) \end{split}$$

... is a sinusoid with amplitude  $\sqrt{\xi_0^2 + \eta_0^2}$  and phase  $\angle(\xi_0, \eta_0)$ .

 $\xi' = \xi_0 \cos \varphi + \eta_0 \sin \varphi$ 





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## Radon transform

(sinogram)

of a square (inverted)



# Radon transform (sinogram)

of an object with inserts (inverted)



Object

Sinogram